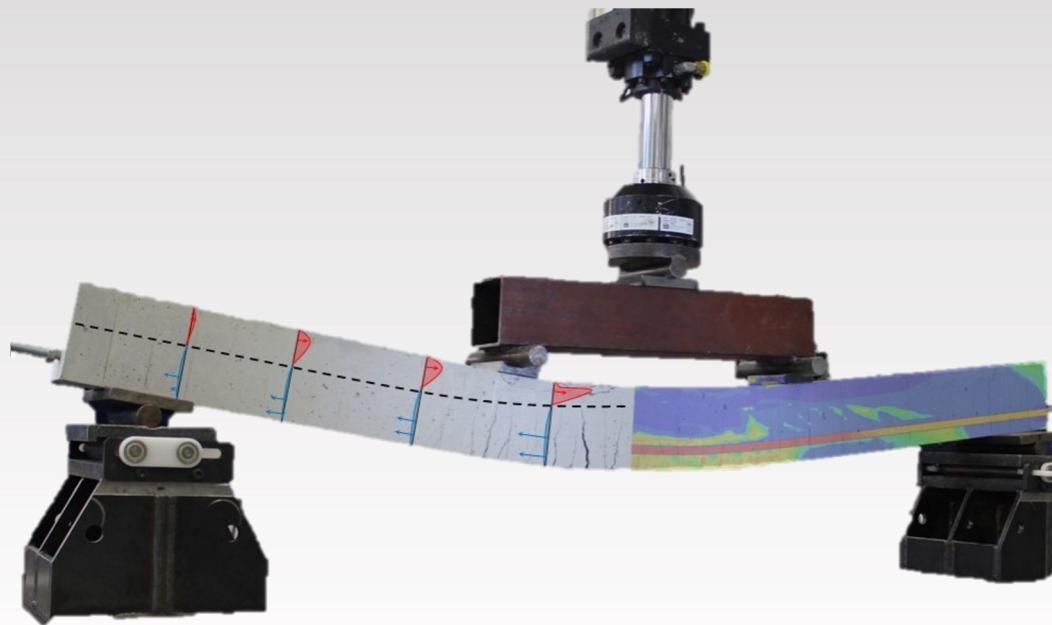


Deformationer af UHPSFRC-bjælker med forspændt armering



Daniel Peter Brosbøl

Rasmus Juul Larsen

Agenda

Målsætning

UHPSFRC

Forsøgsserie

Finit element-metoden

Semi-analytisk model

Resultater

Agenda

Målsætning

UHPSFRC

Forsøgsserie

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Semi-analytisk model

Resultater

Målsætning

1. Modellering af opspændte UHPSFRC bjælker
2. Indflydelsen af opspænding
3. Sammenligning af modeller og forsøgsresultater

Målsætning

1. Modellering af opspændte UHPSFRC bjælker
2. Indflydelsen af opspænding
3. Sammenligning af modeller og forsøgsresultater

UHPSFRC

UHPC

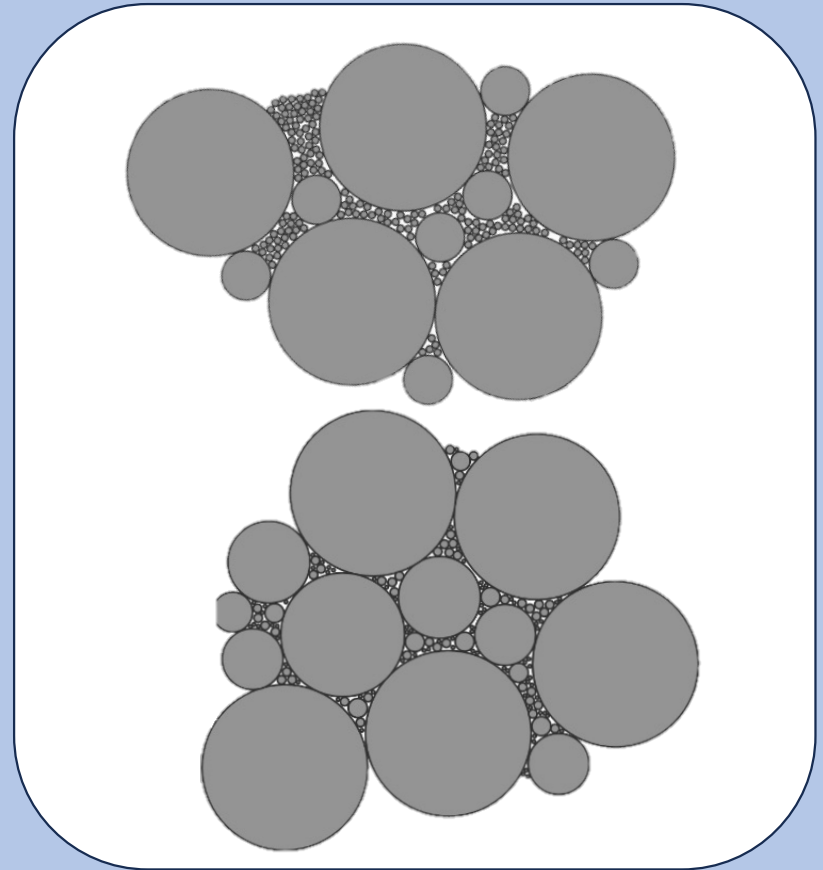
Fibre

Styrke parametre

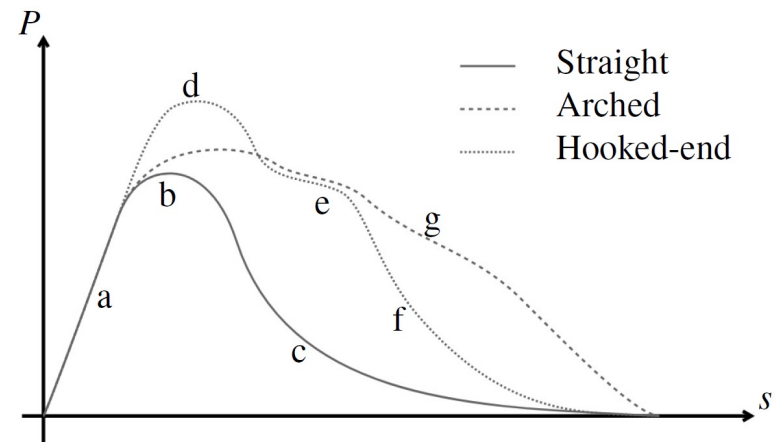
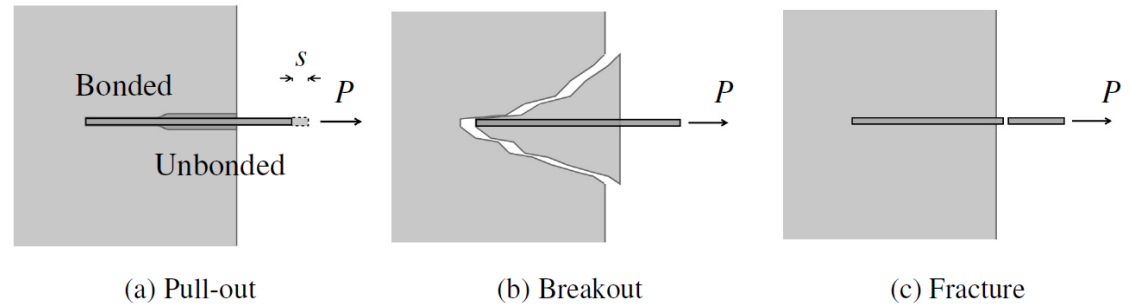
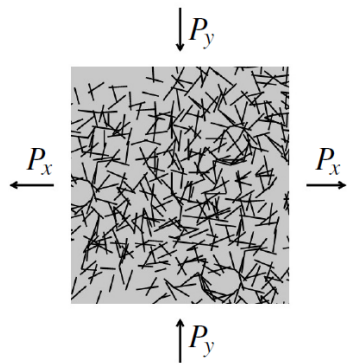
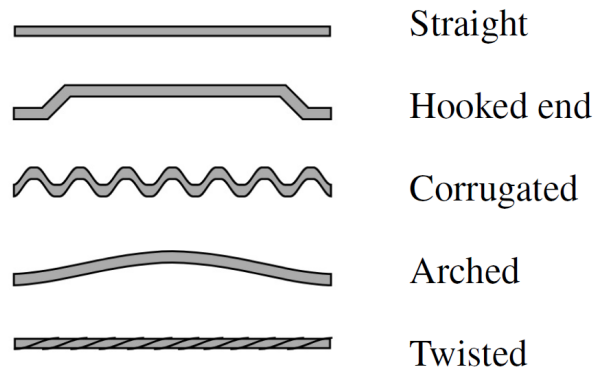
Opspændte Bjælker



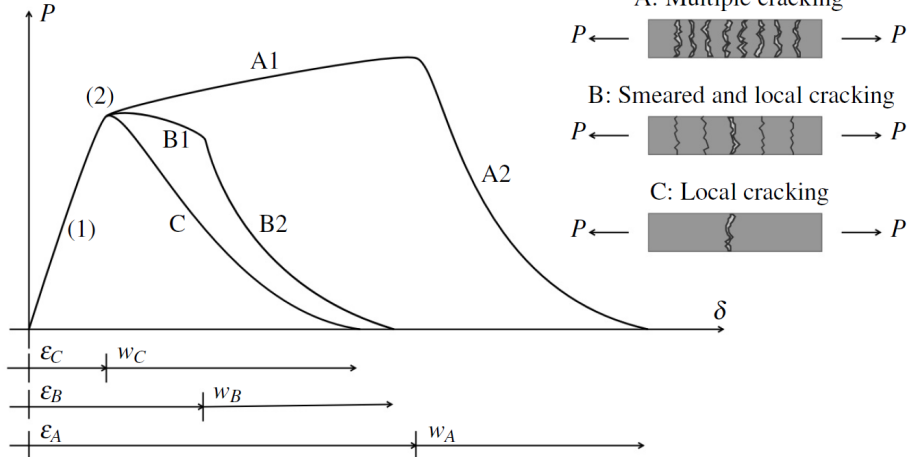
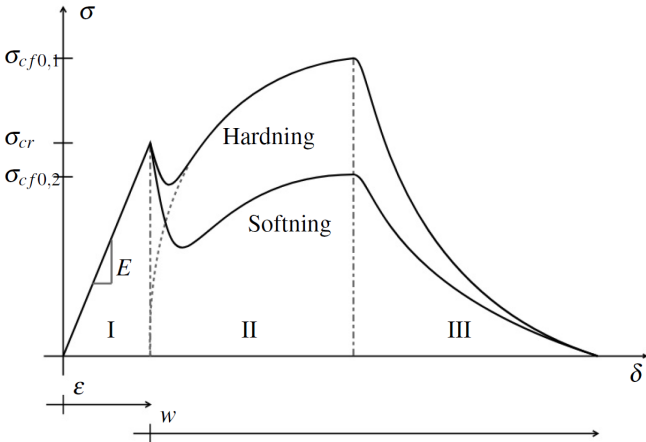
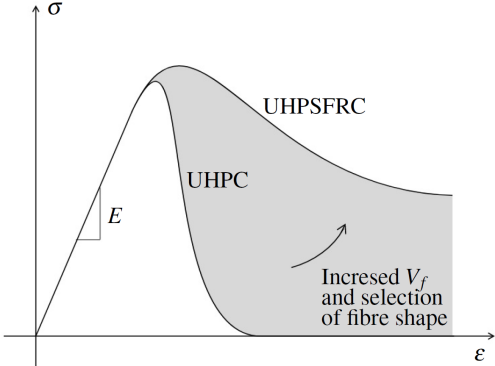
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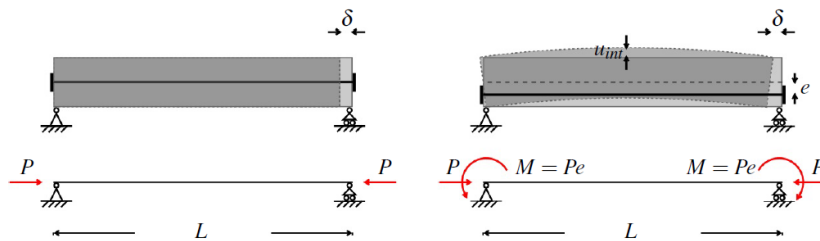
Fibre



Styrke parametre

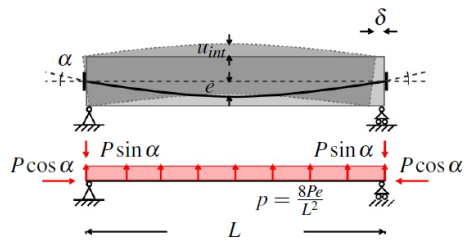


Opspændte bjælker

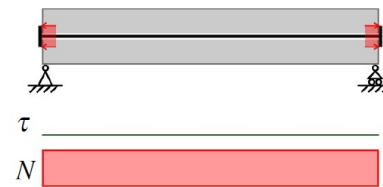


(a) Centered Tendon

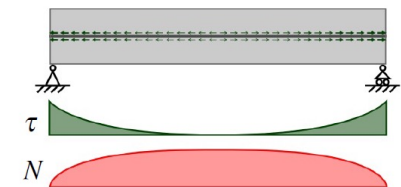
(b) Eccentric Tendon



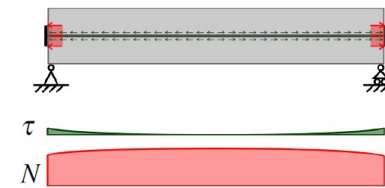
(c) Parabolic Tendon



(a) Normal transfer



(b) Shear transfer



(c) Normal transfer and shear transfer

Forsøgsserie

Cylinder trykforsøg

G_F -bjælke bøjningsforsøg

Trækforsøg af armering

Bjælke forsøg

Forsøgsserie

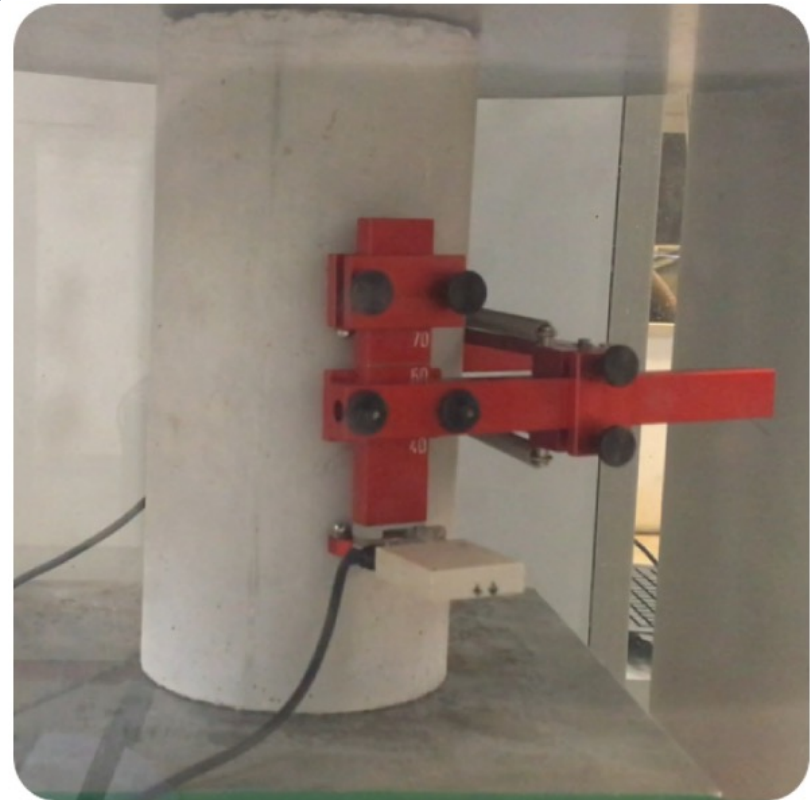
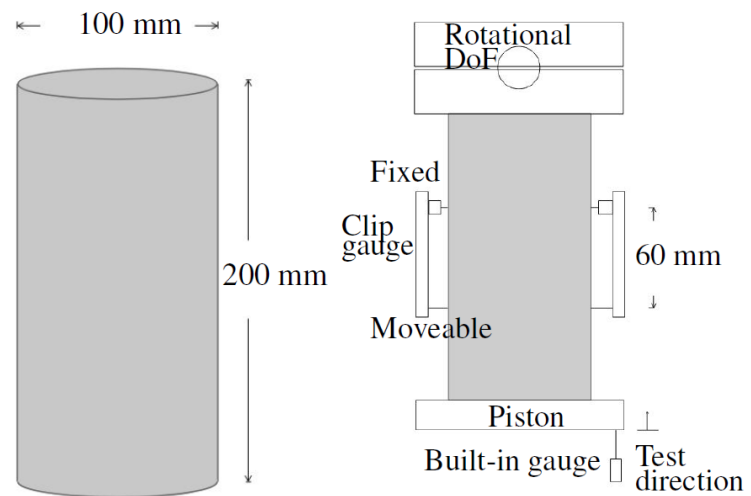
Cylinder trykforsøg

G_F -bjælke bøjningsforsøg

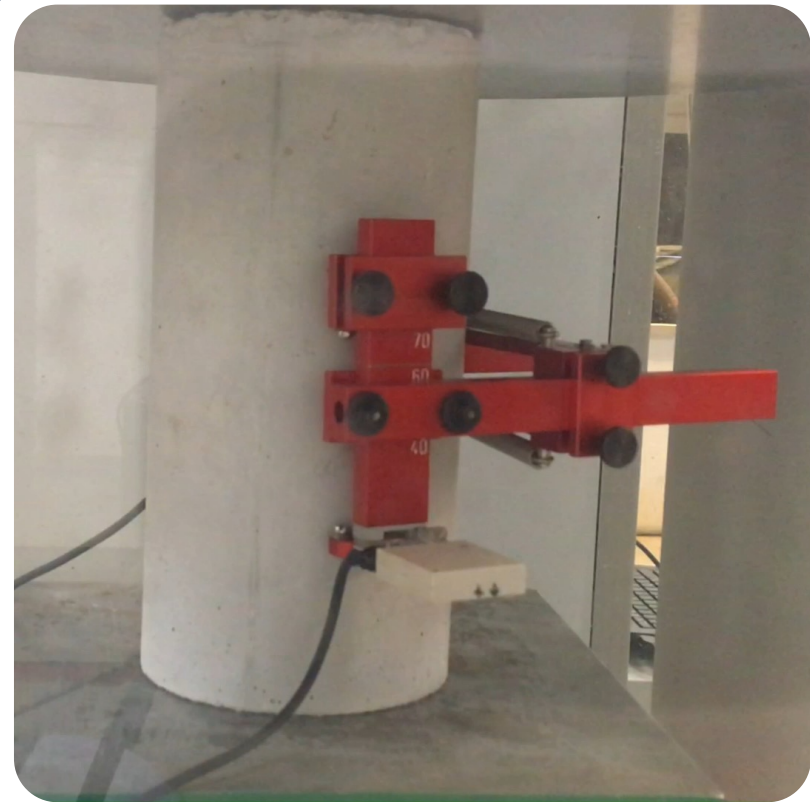
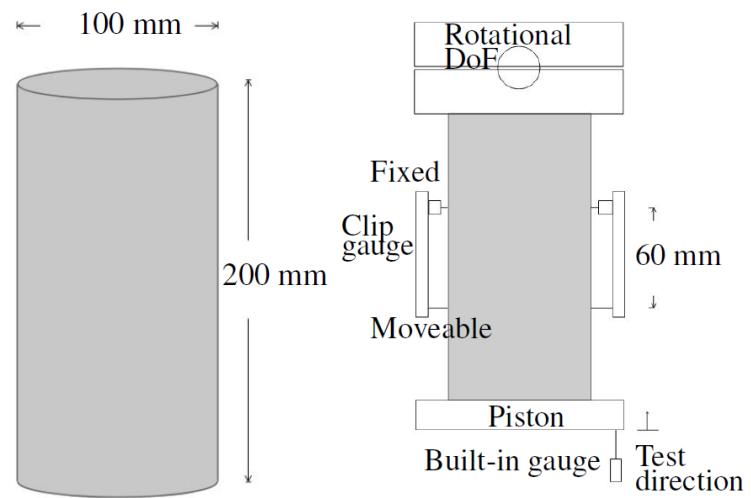
Trækforsøg af armering

Bjælke forsøg

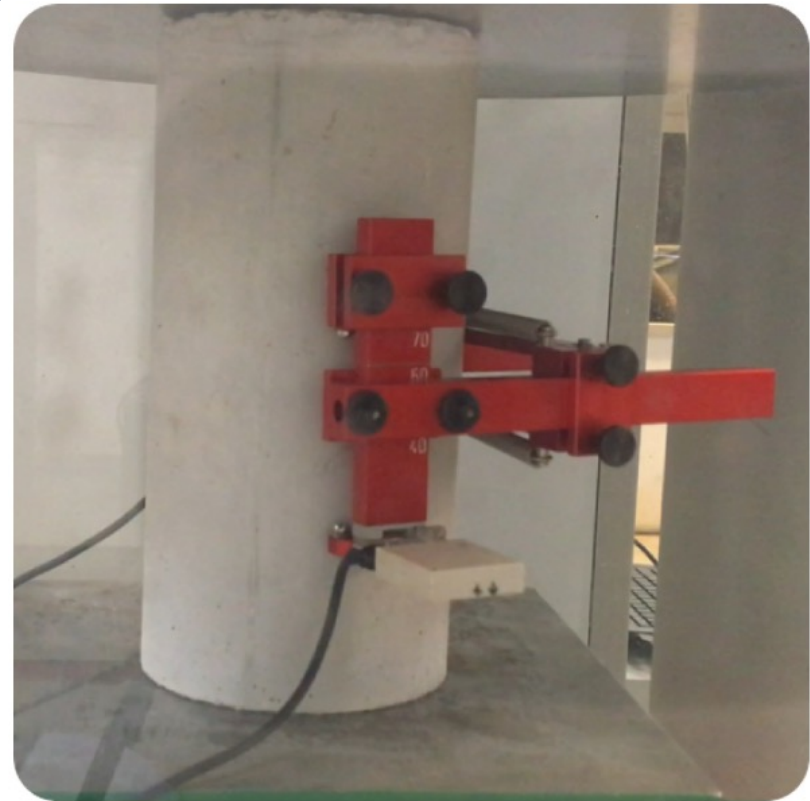
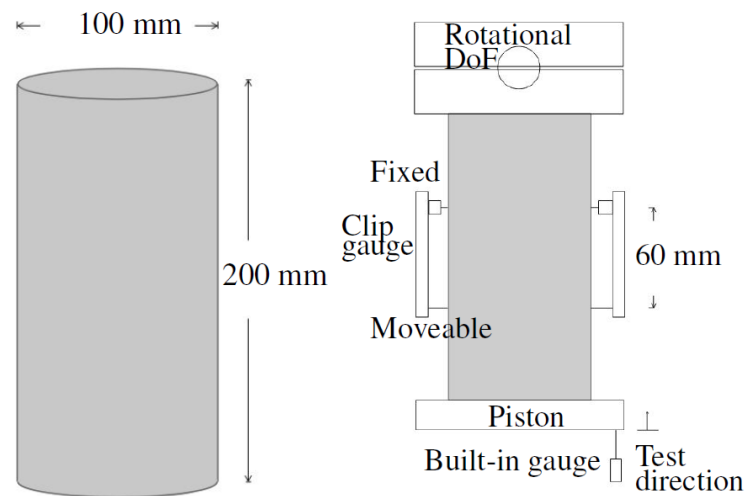
Cylinder trykforsøg



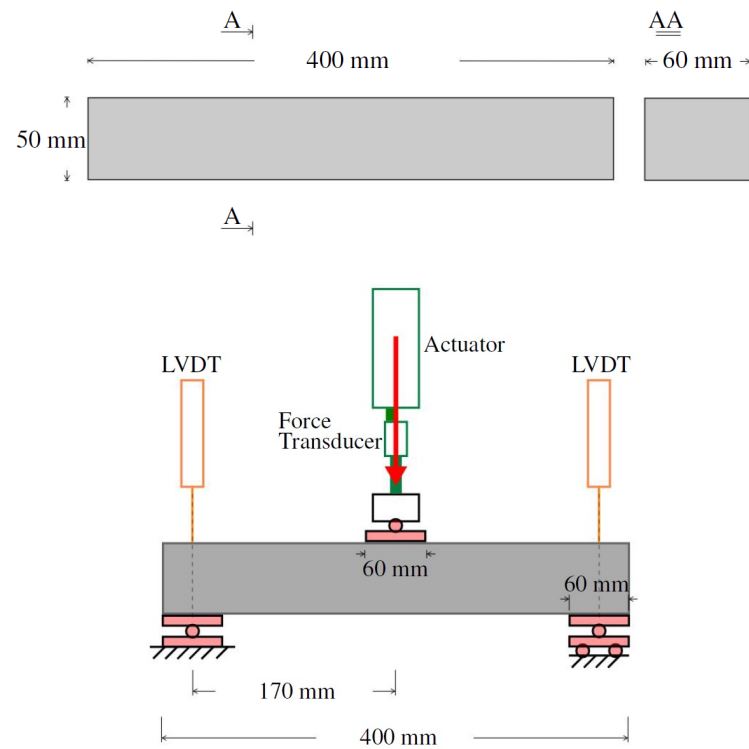
Cylinder trykforsøg



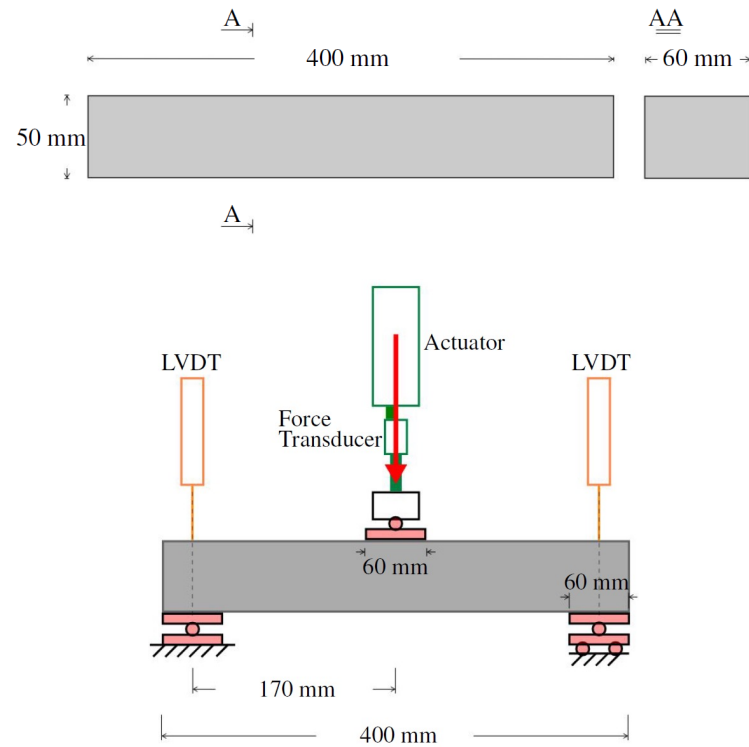
Cylinder trykforsøg



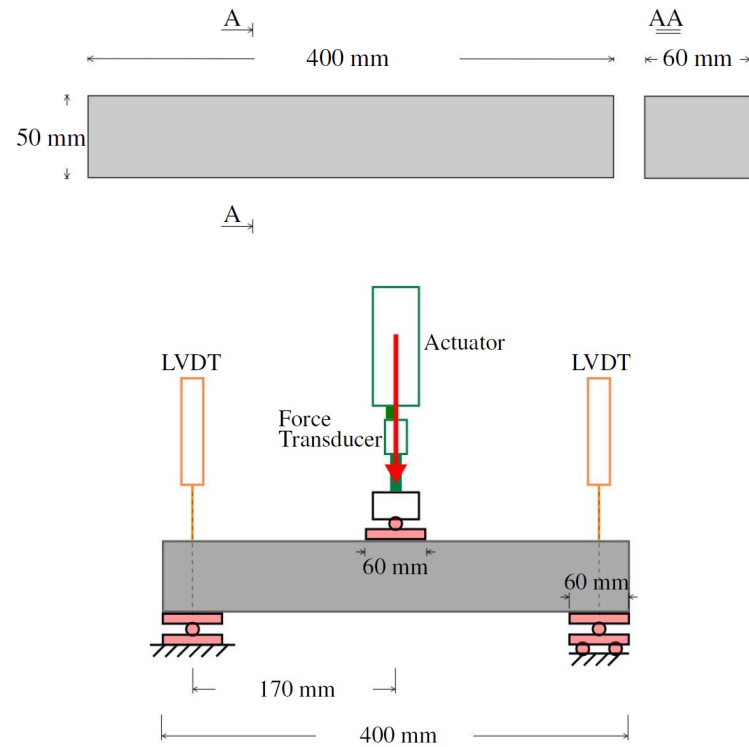
G_F -bjælke bøjningsforsøg



G_F -bjælke bøjningsforsøg



G_F -bjælke bøjningsforsøg



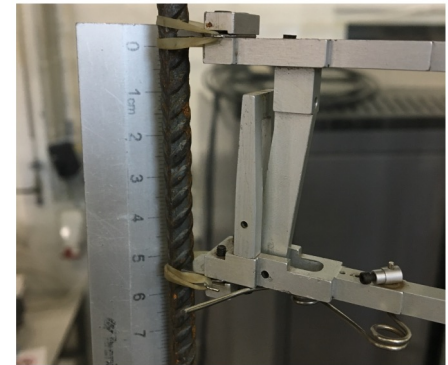
Trækforsøg af armering



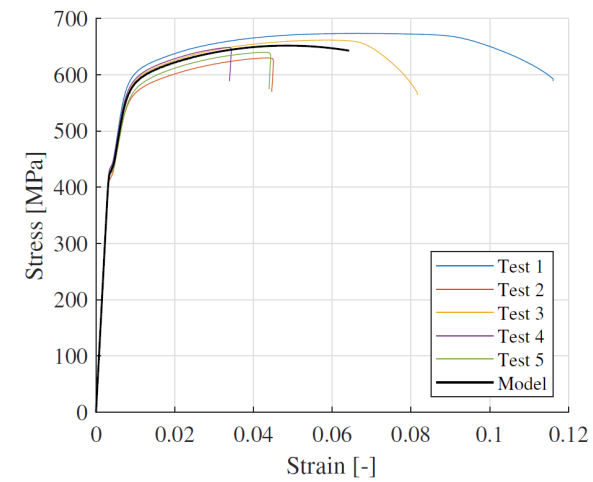
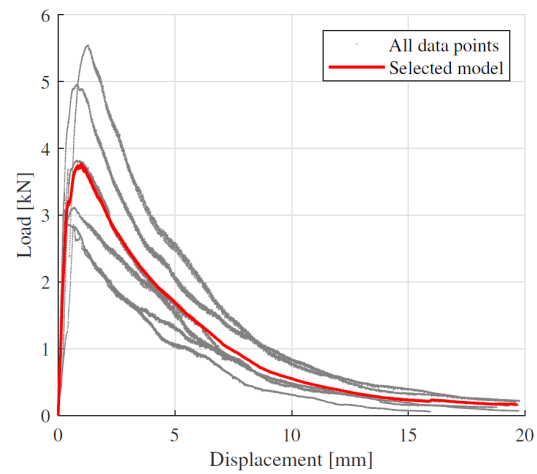
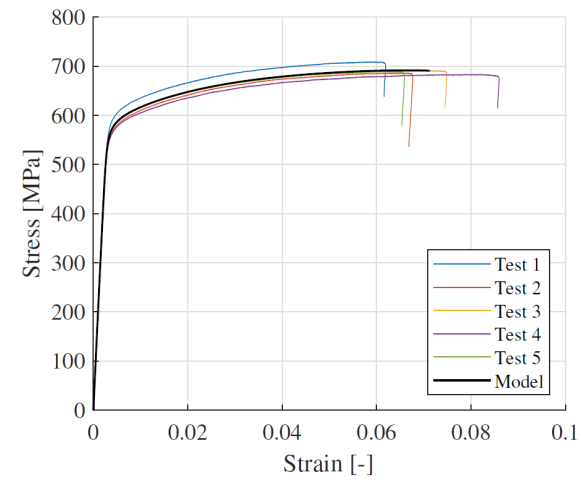
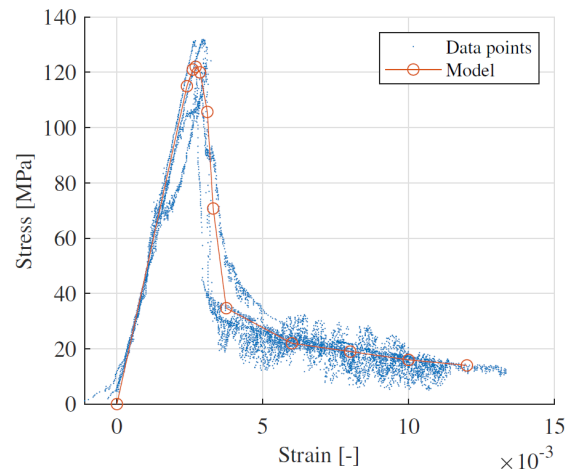
(a) Rebar



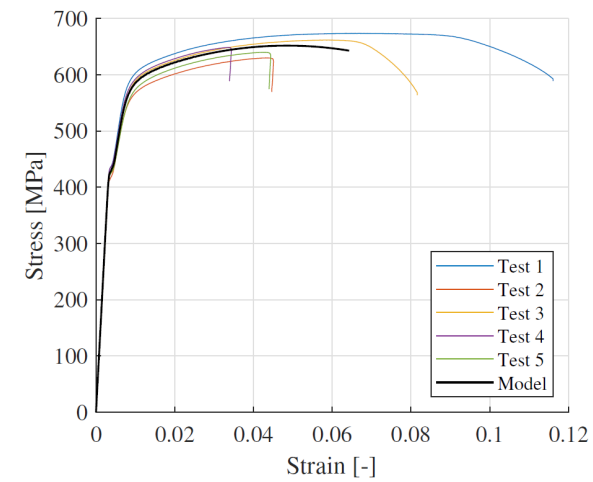
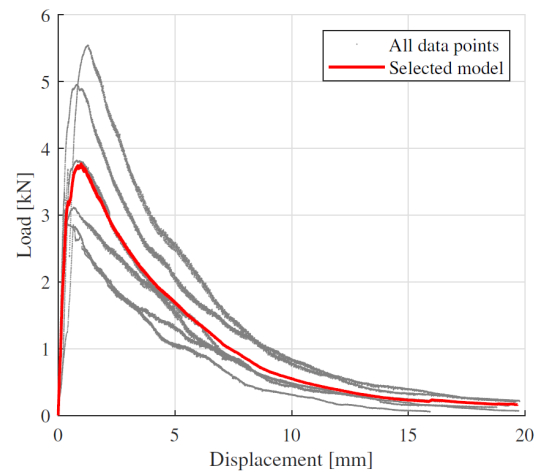
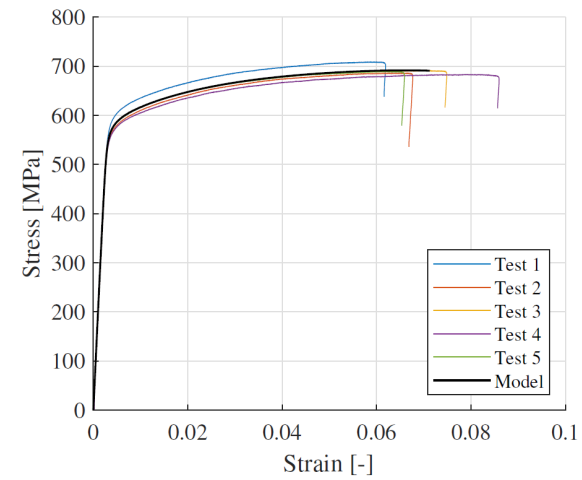
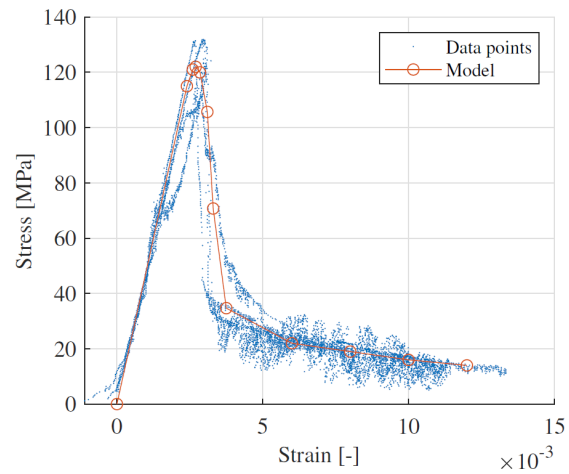
(b) Threaded rod



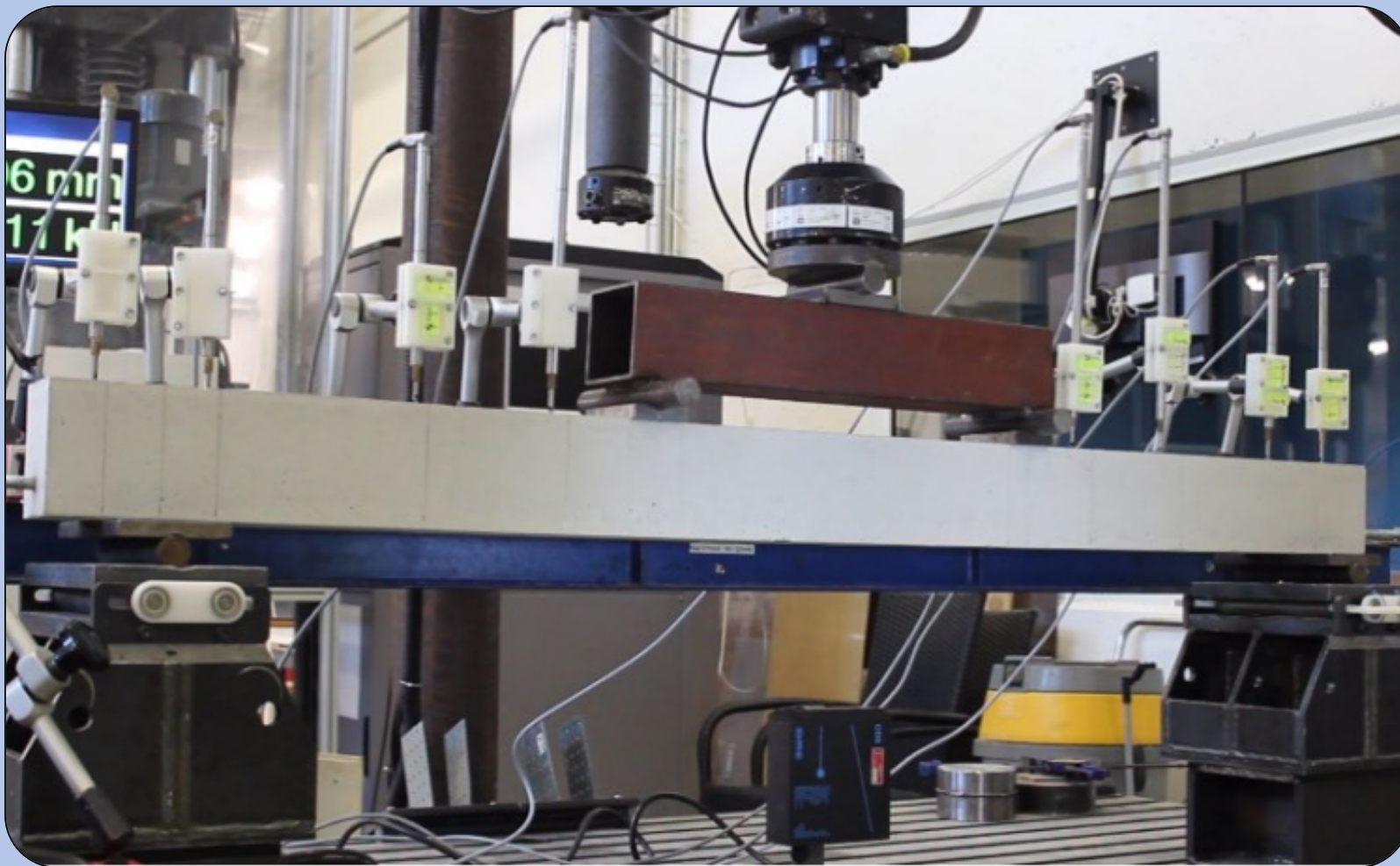
Data til modeller



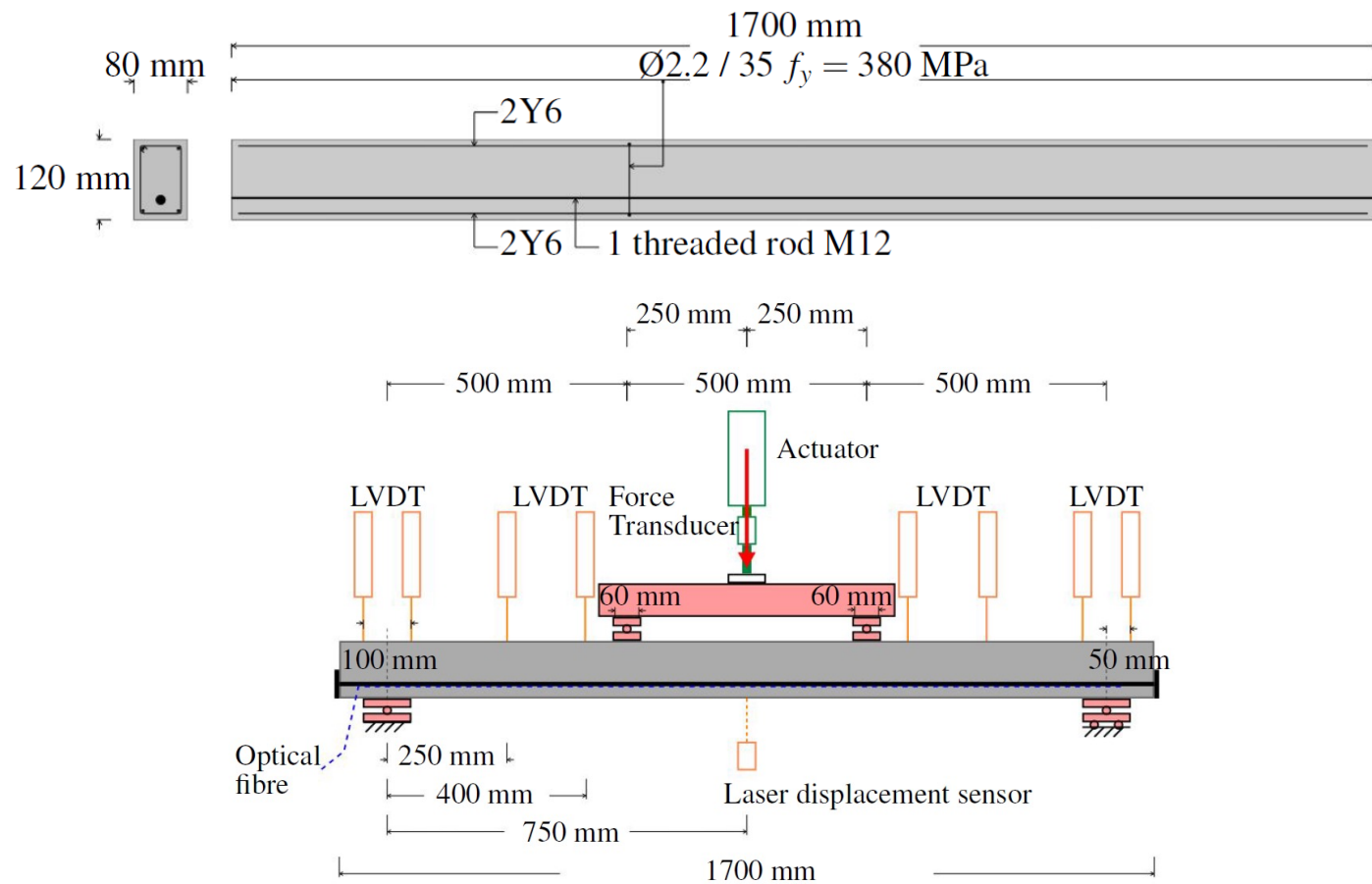
Data til modeller



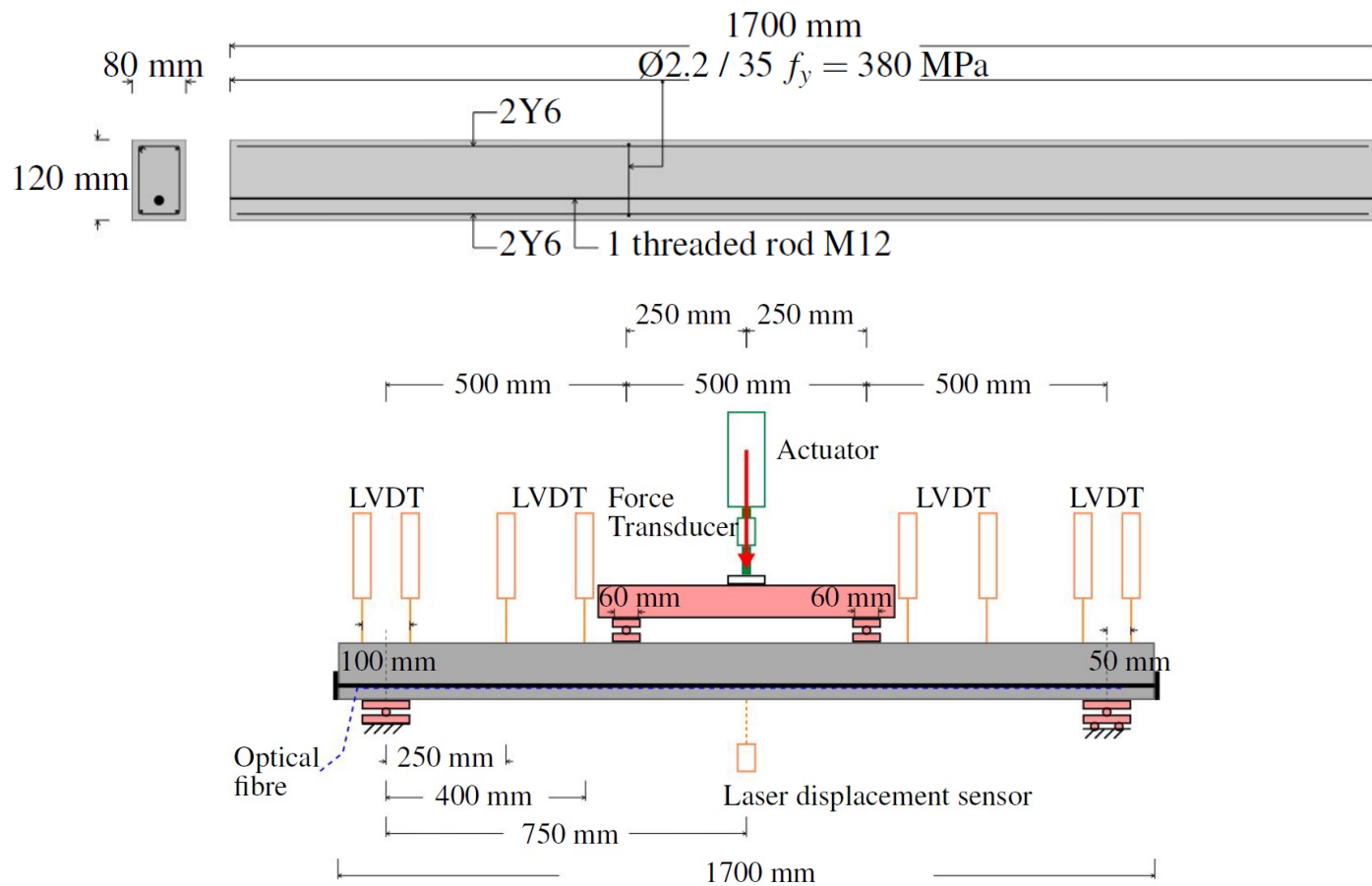
Bjælkeforsøg



Forsøgsopstilling



Forsøgsopstilling



Forberedelse

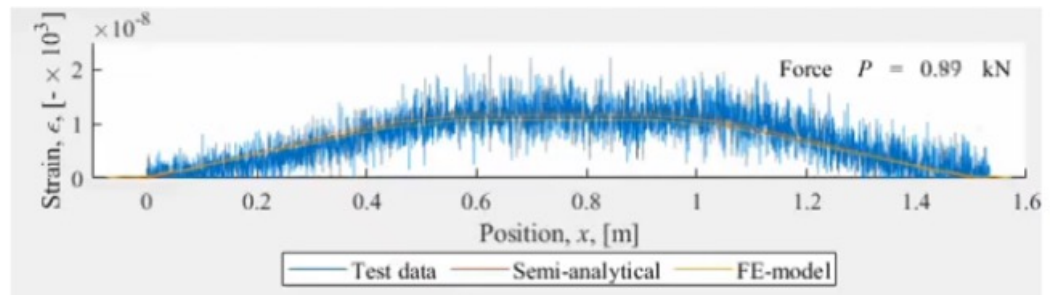
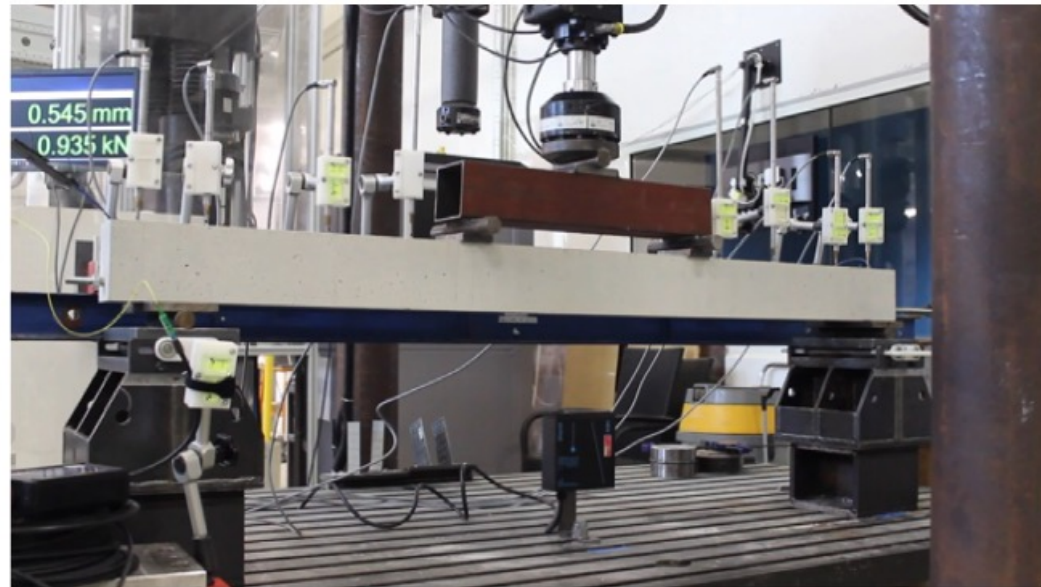
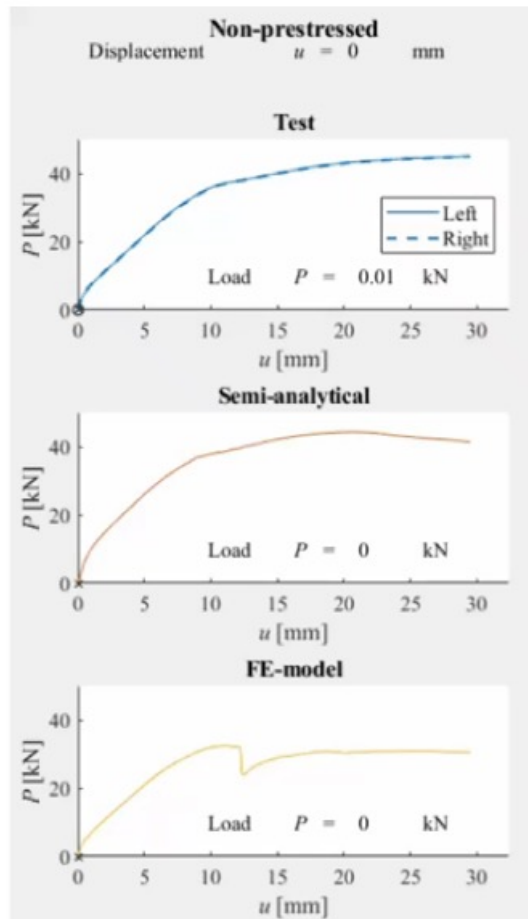
Armeringsarbejde

Opspænding

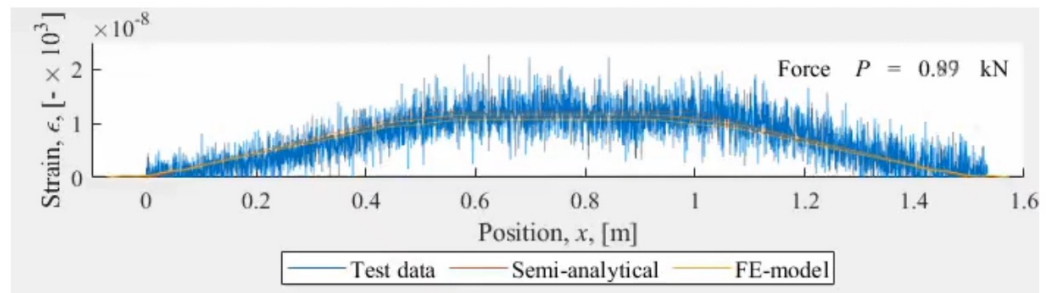
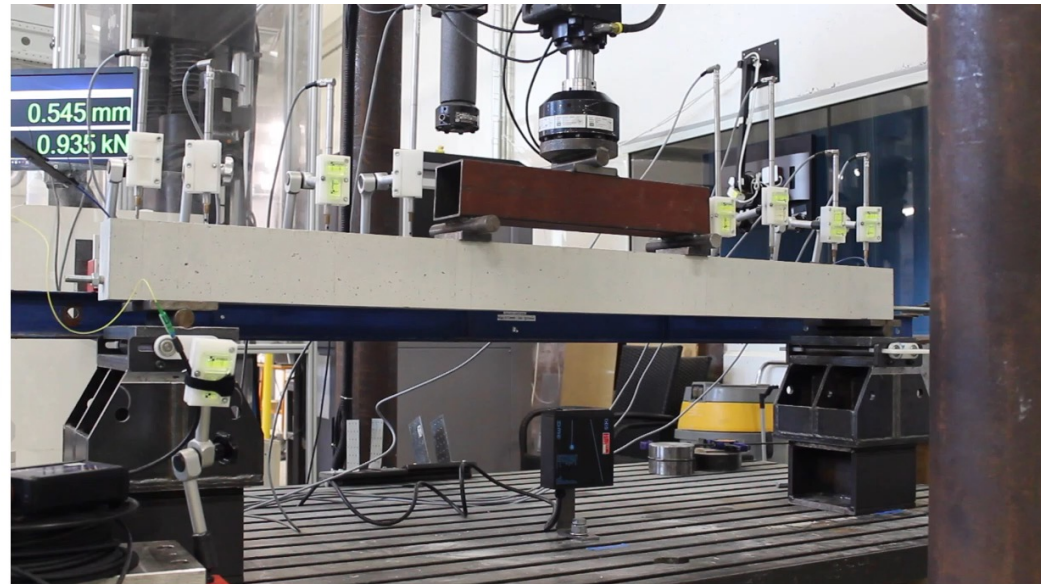
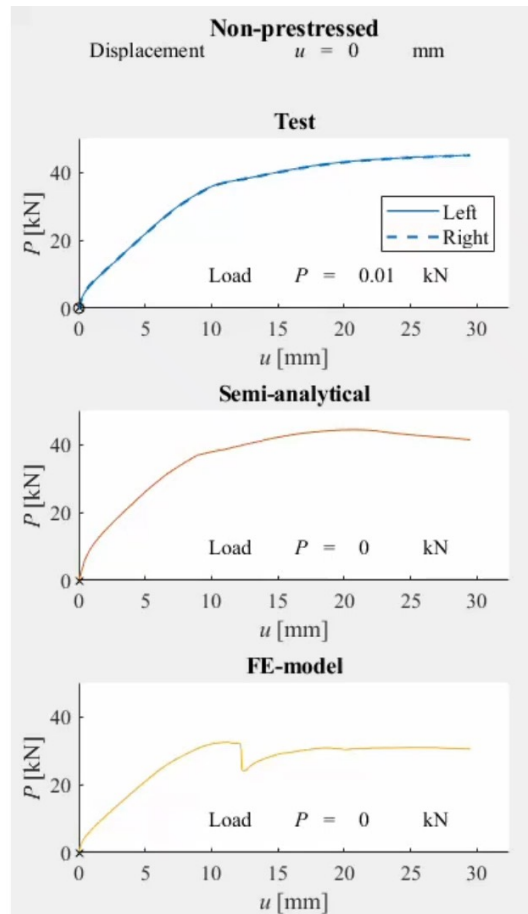
Støbning



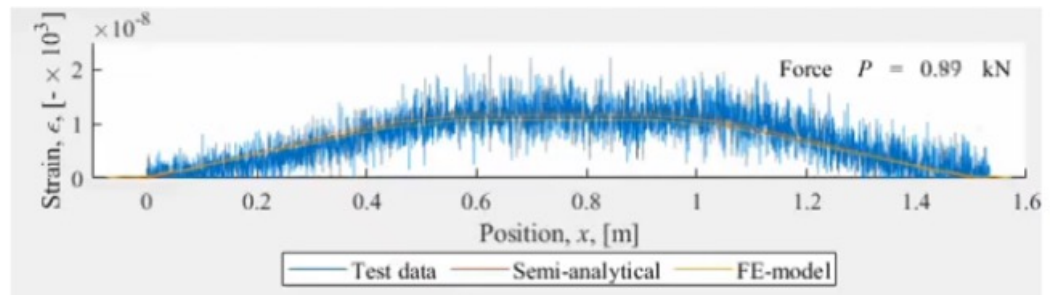
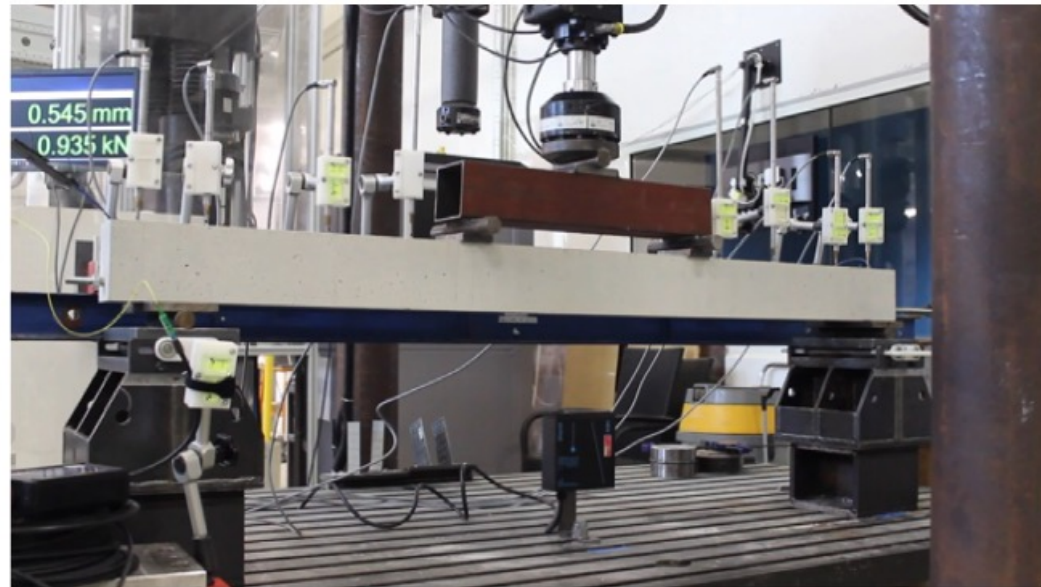
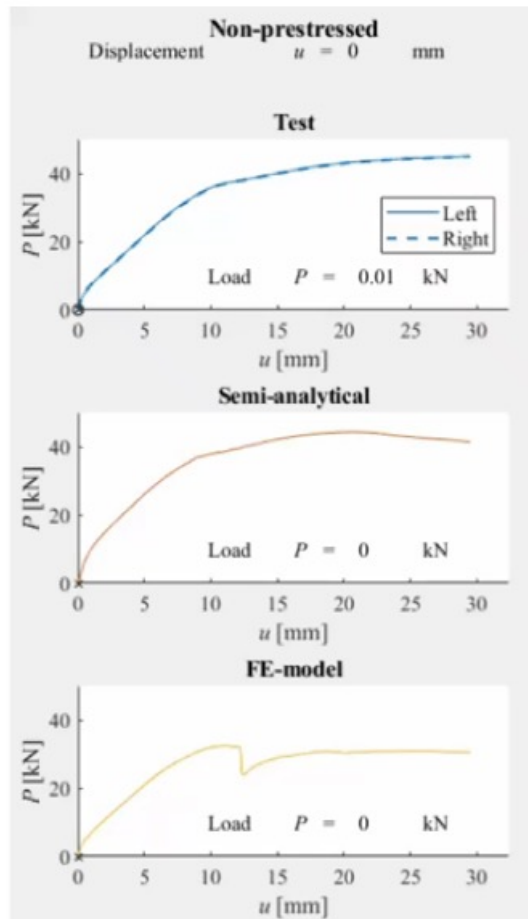
Slapt armeret



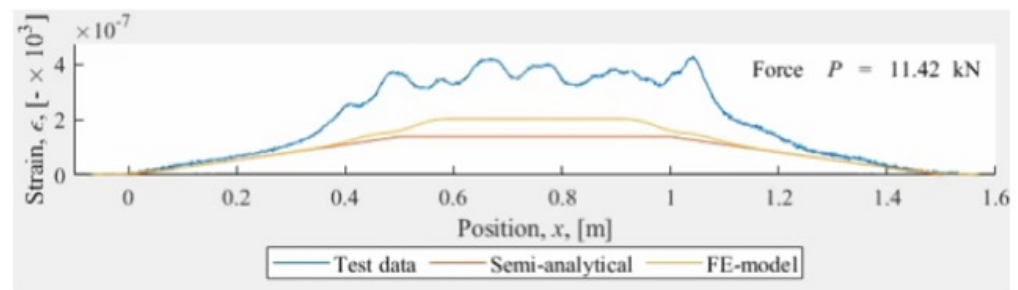
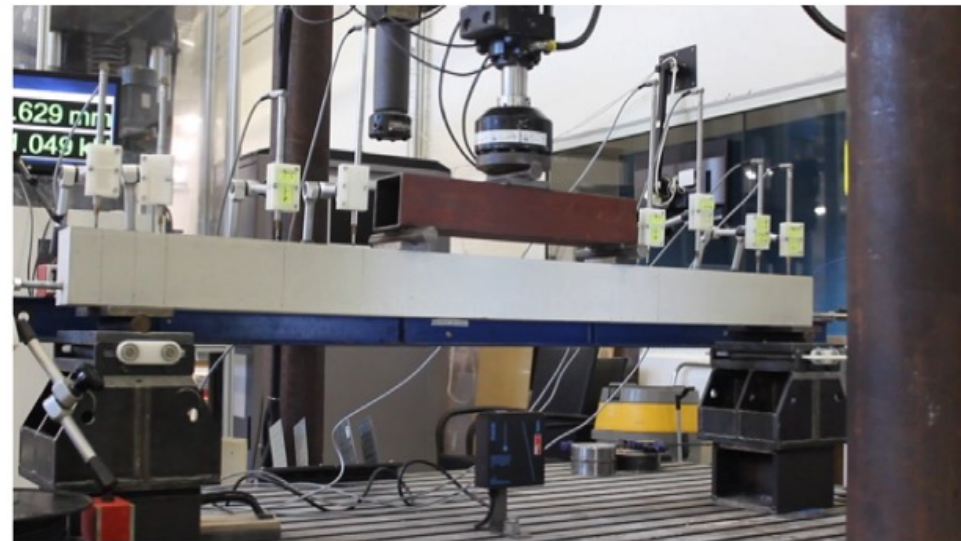
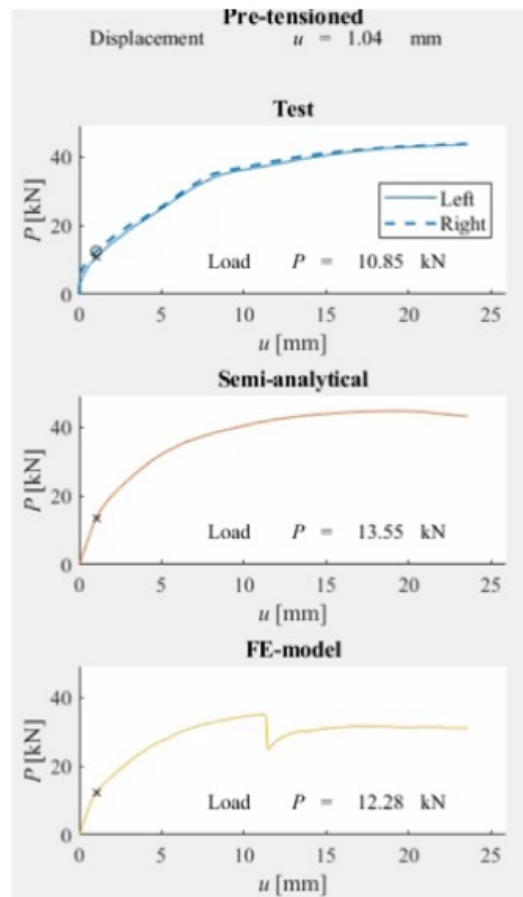
Slapt armeret



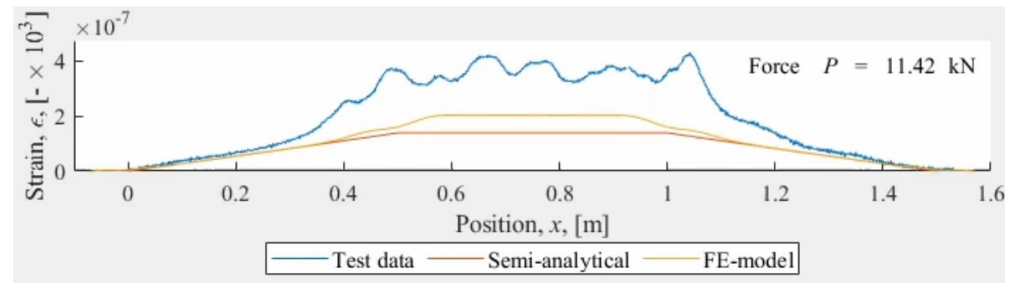
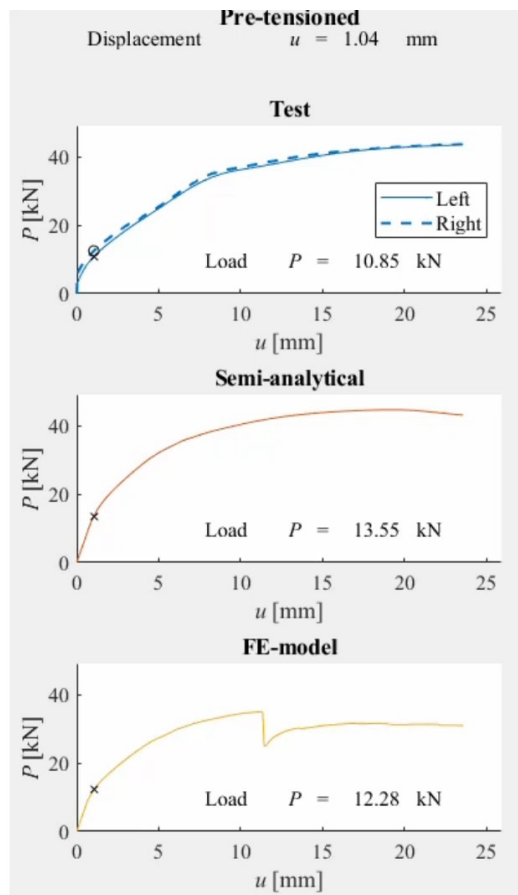
Slapt armeret



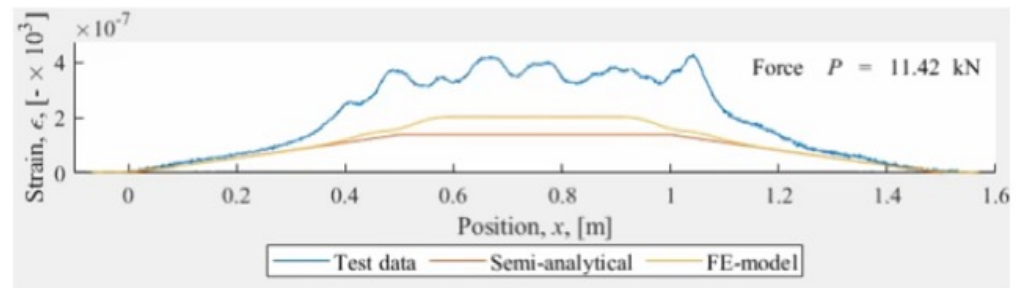
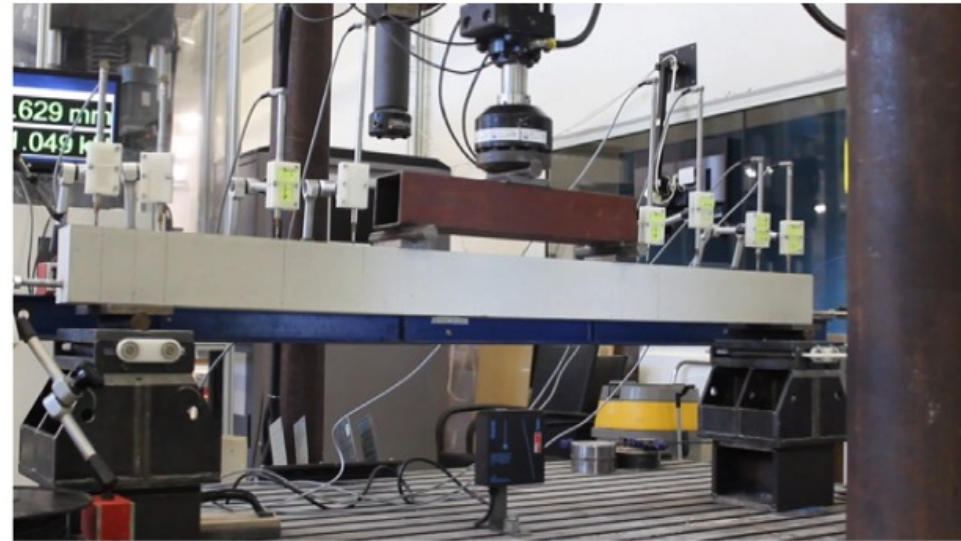
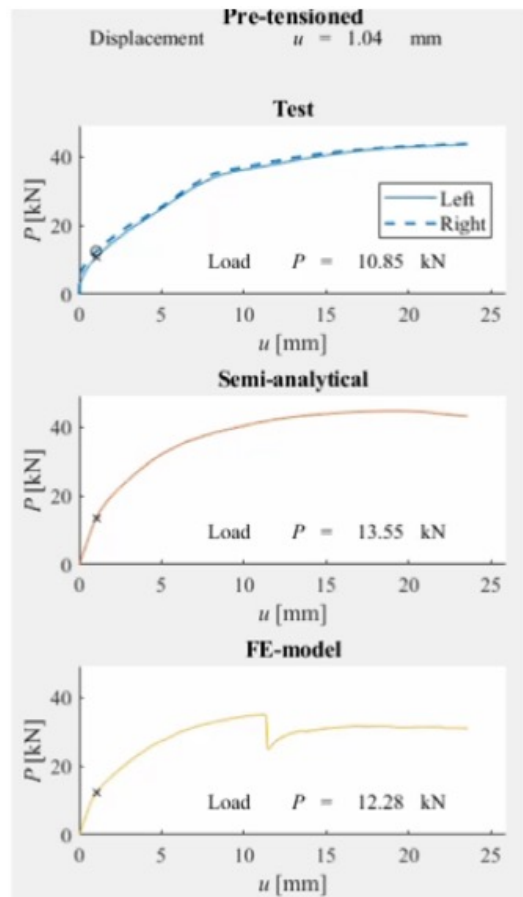
Før-spændt



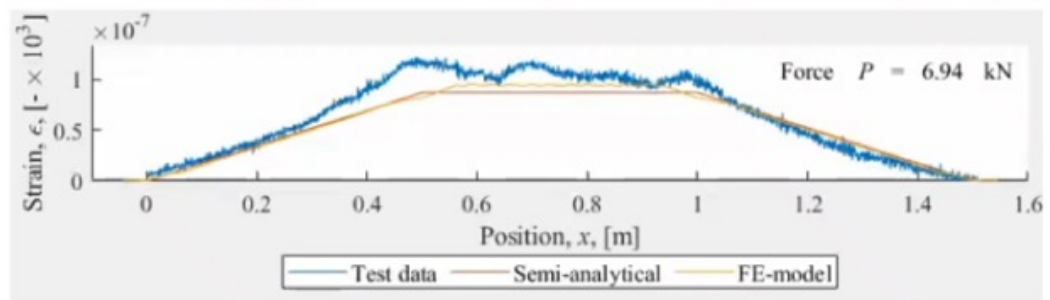
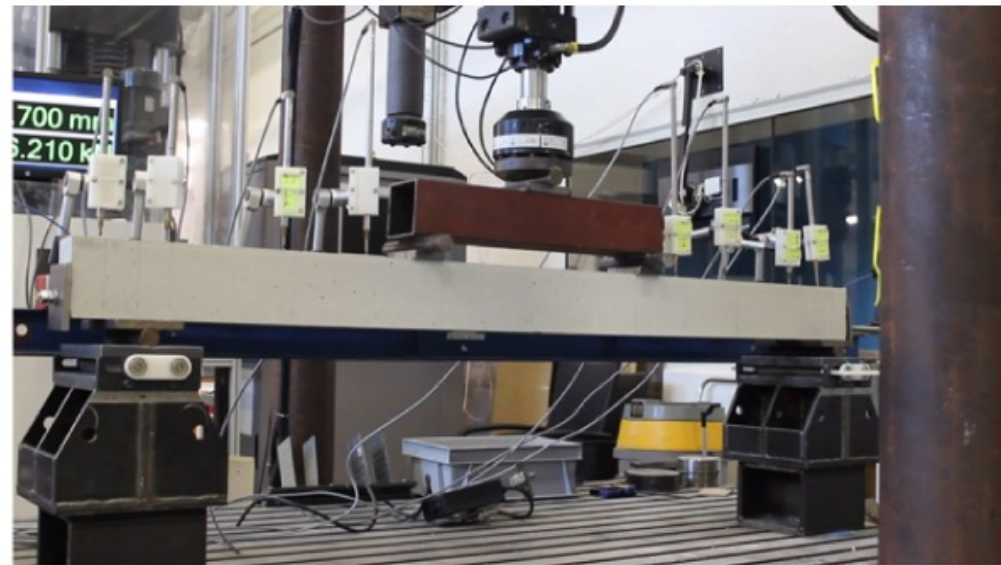
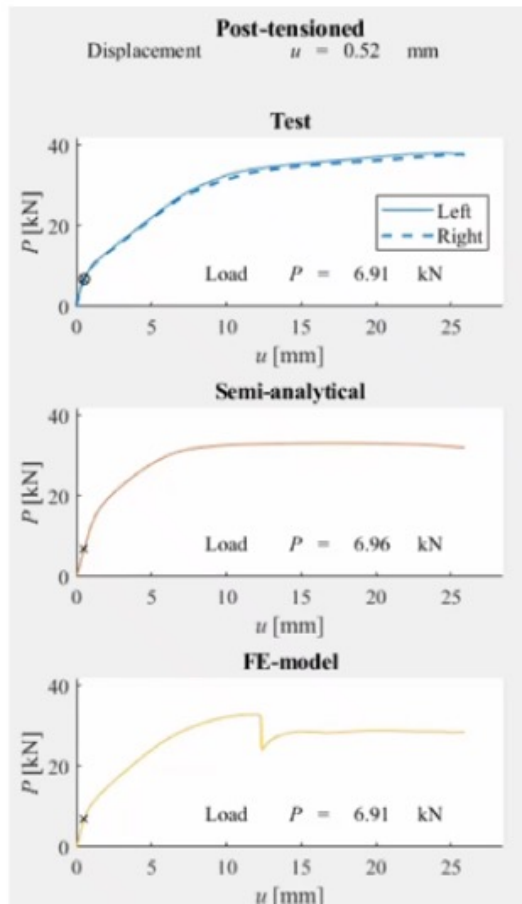
Før-spændt



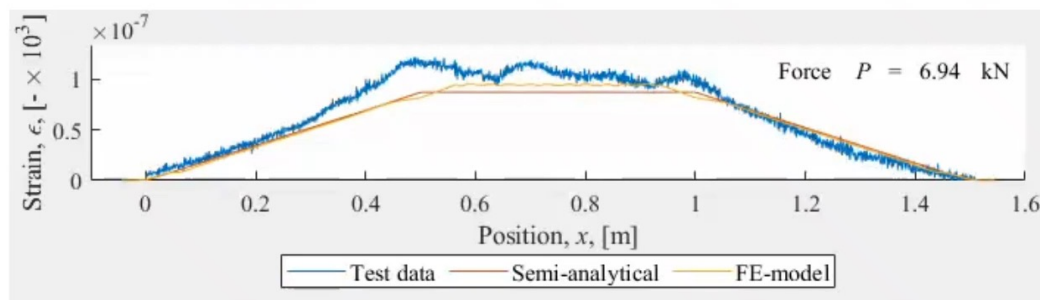
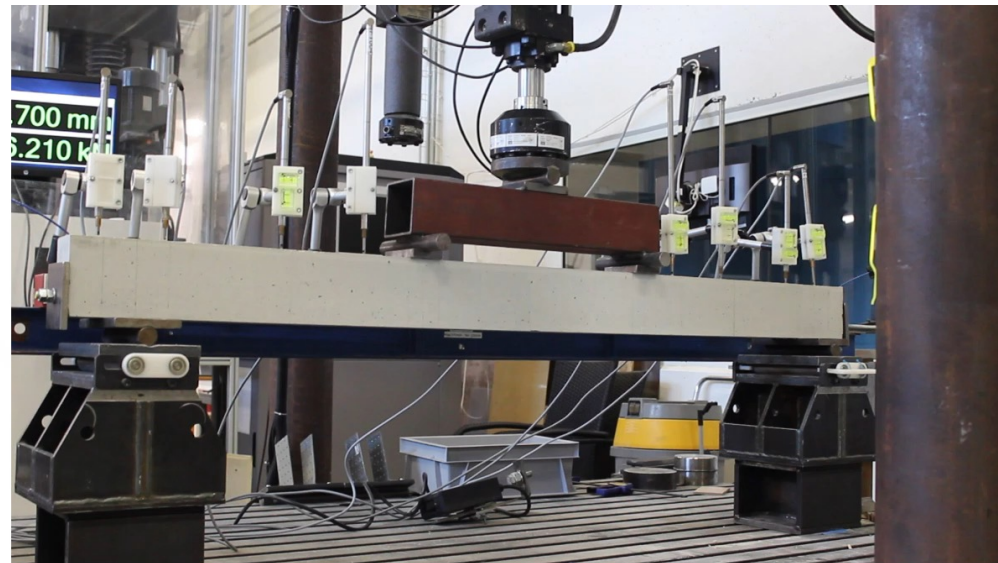
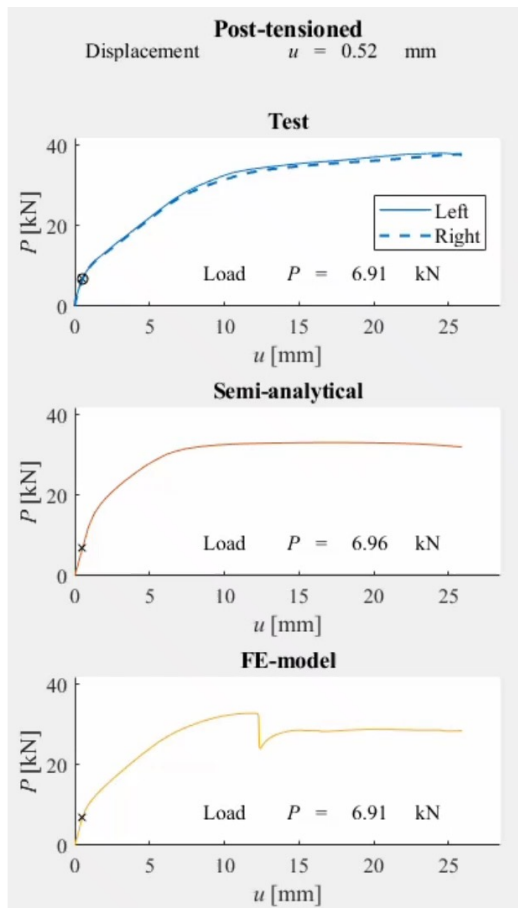
Før-spændt



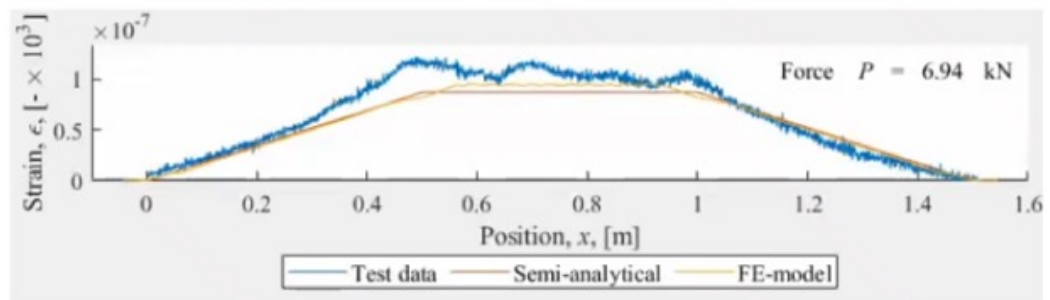
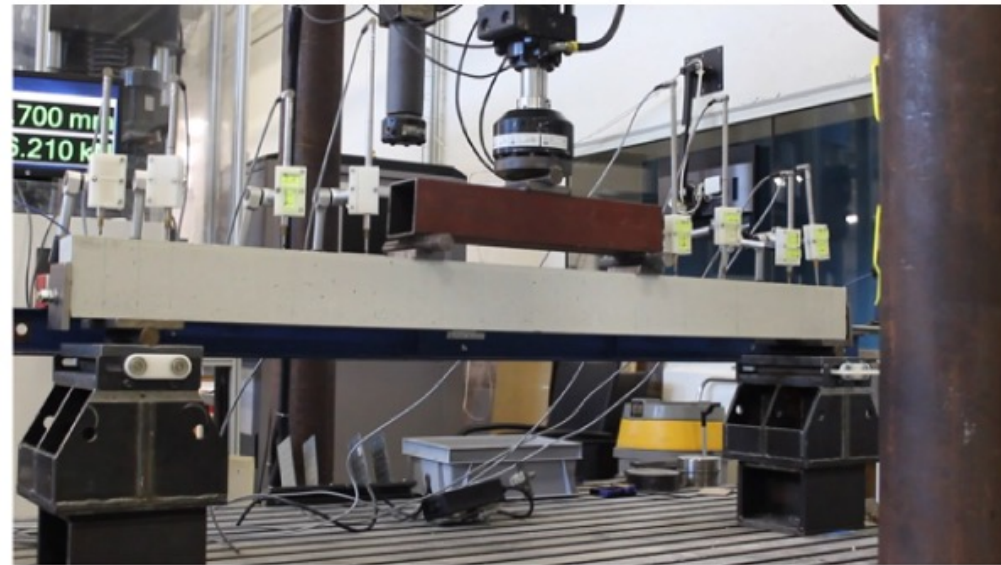
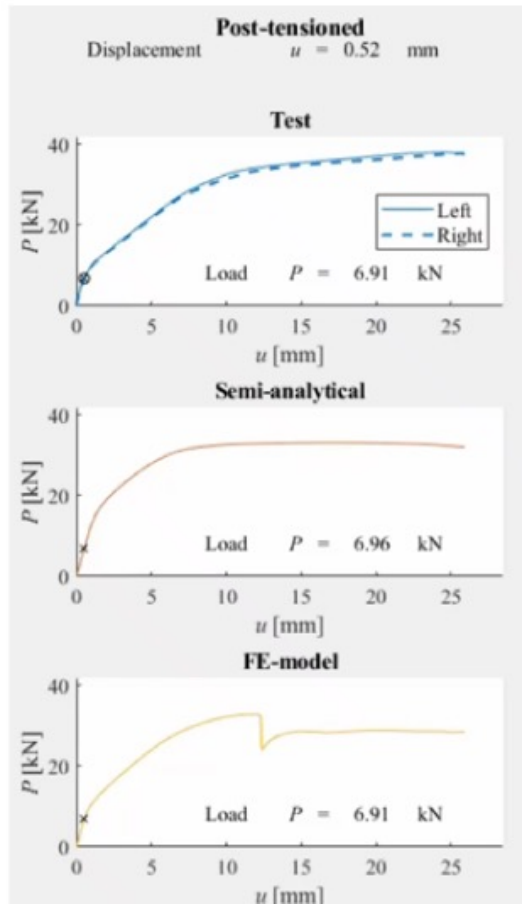
After-spændt



After-spændt



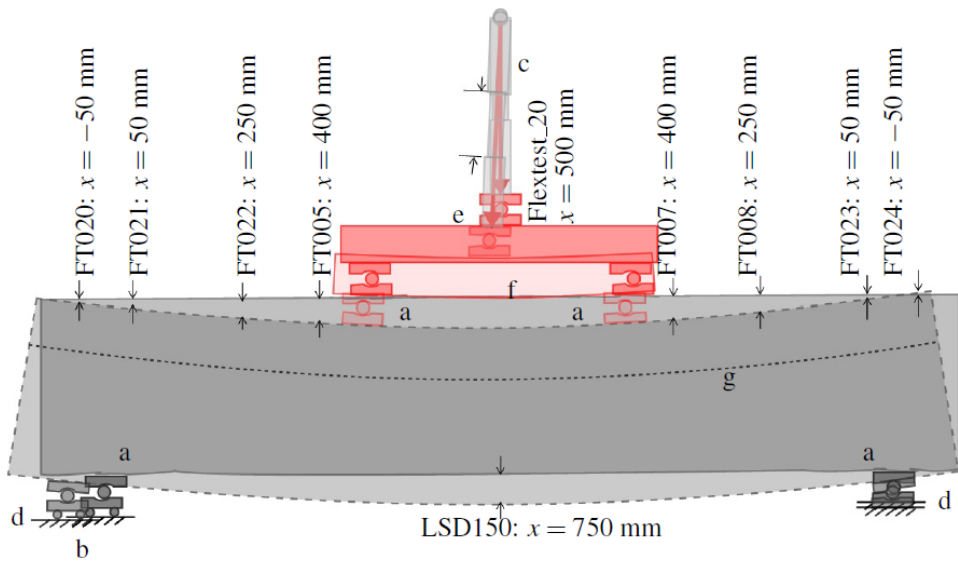
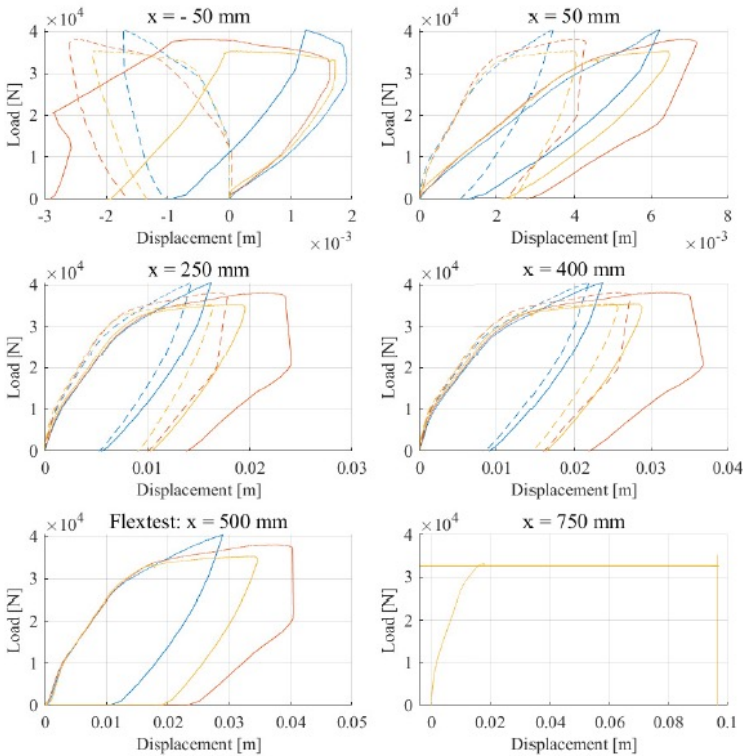
After-spændt



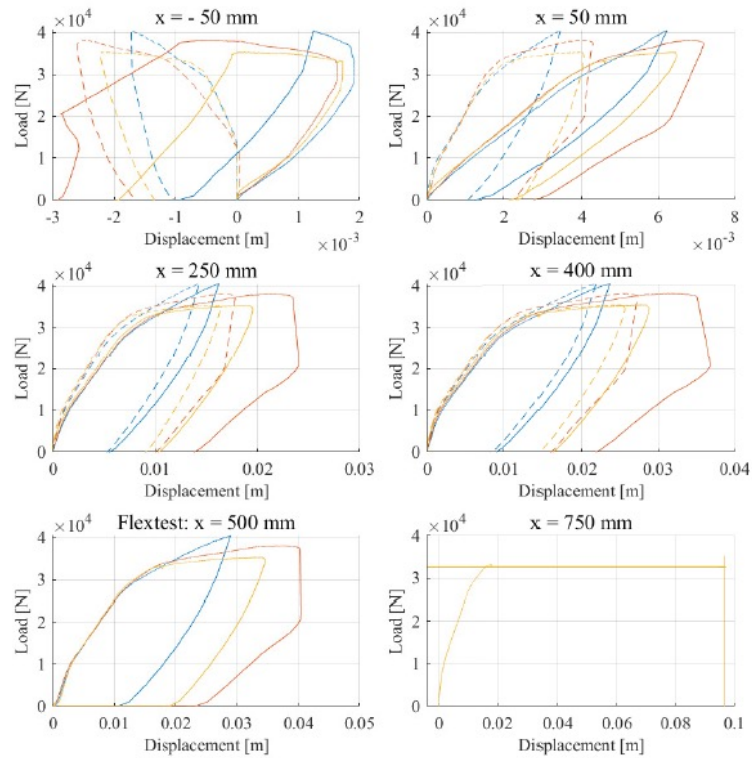
Revnemønster



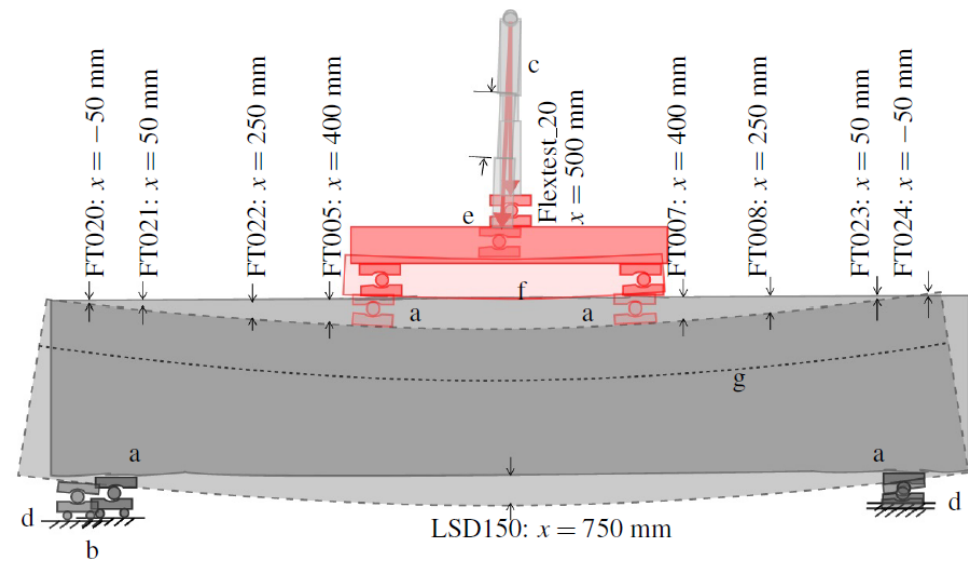
Optaget data



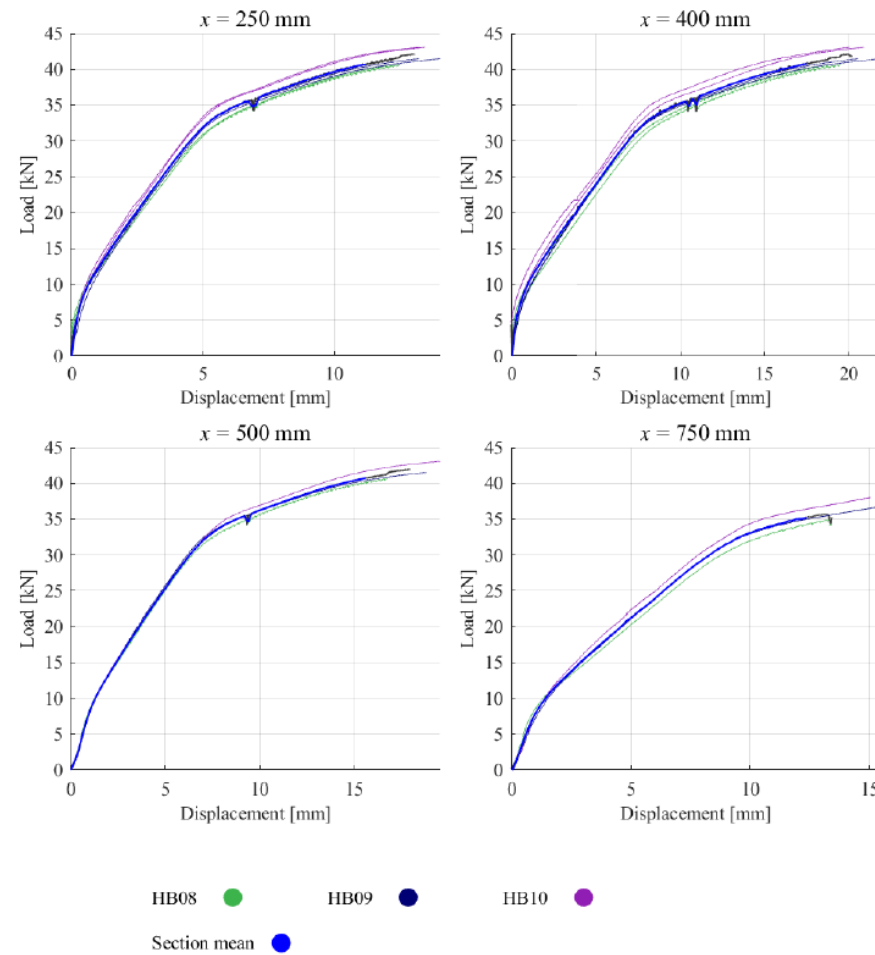
Optaget data



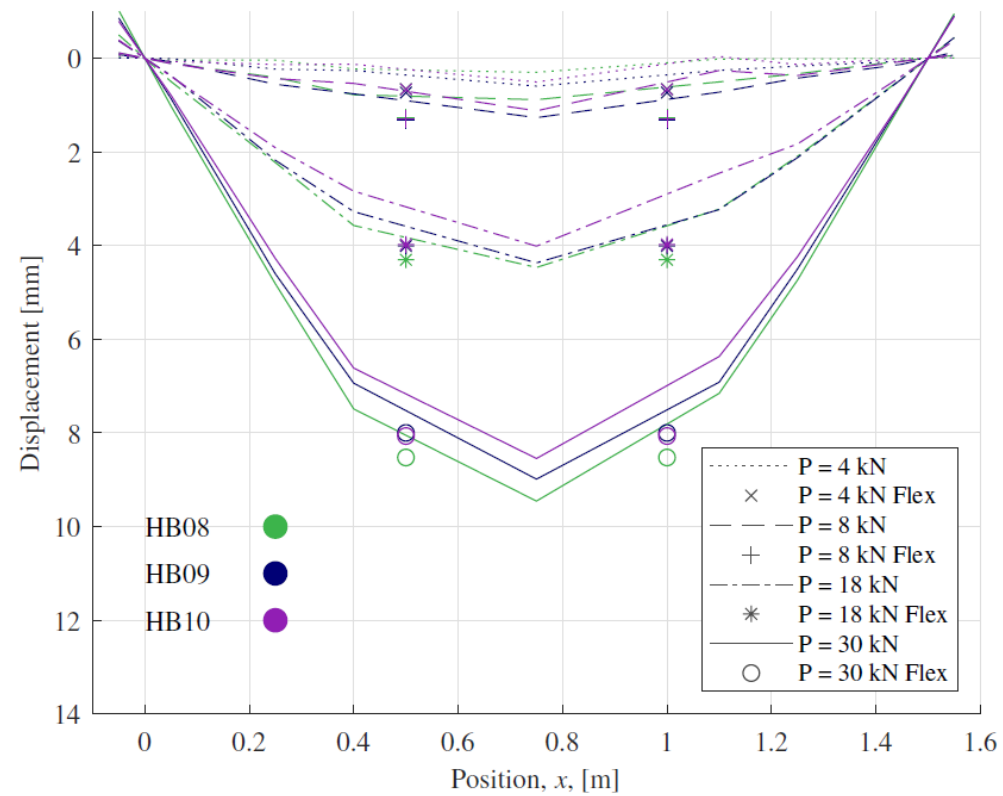
Beams id:	Left LVDT	Right LVDT
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HB09	— (solid orange)	- - - (dashed orange)
HB10	— (solid yellow)	- - - (dashed yellow)



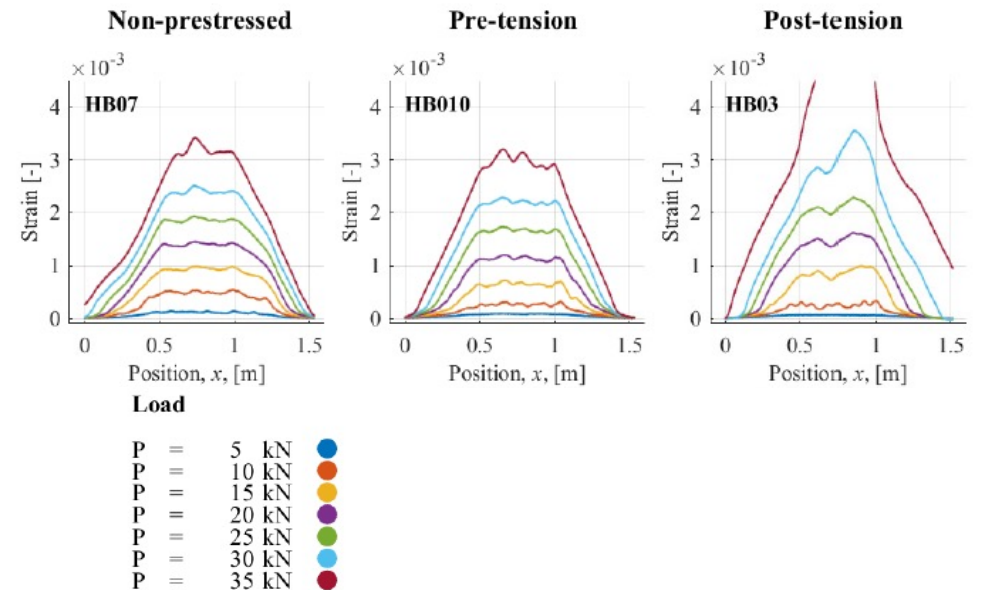
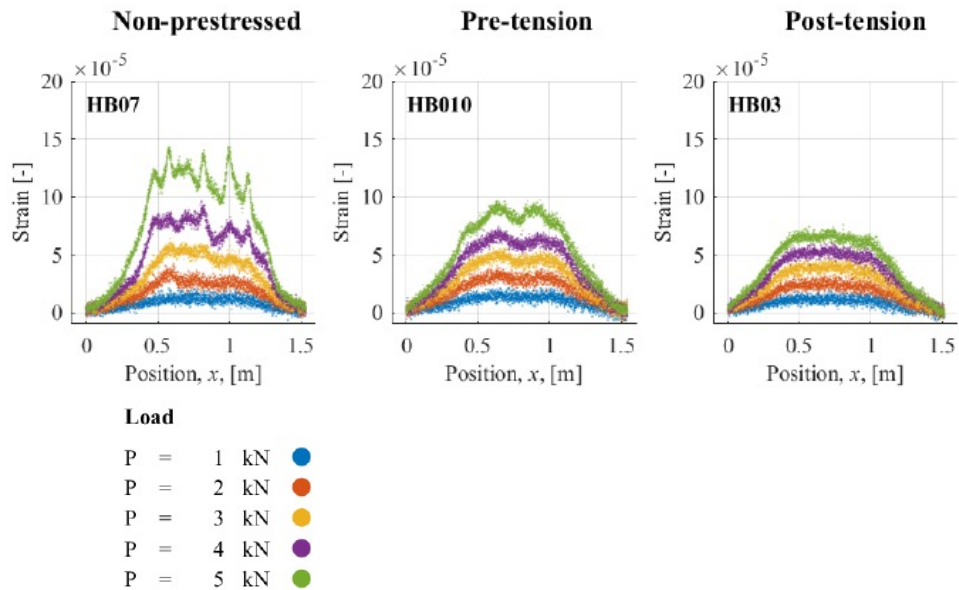
Arbejdskurve



Deformationsfigur



Tøjningsfordeling



Finit element-metoden

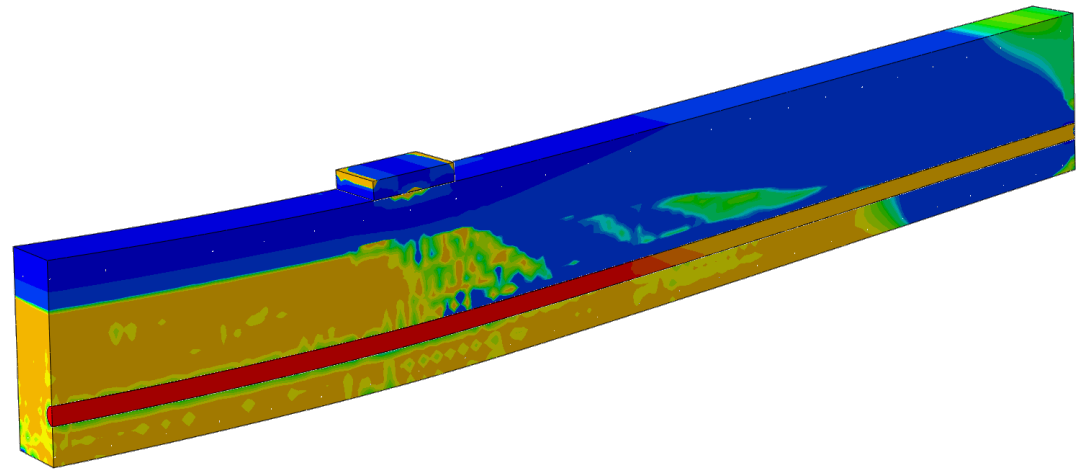
Concrete Damaged Plasticity

Elementer

Randbetingelser

Resultater

Parameter studie



Finit element-metoden

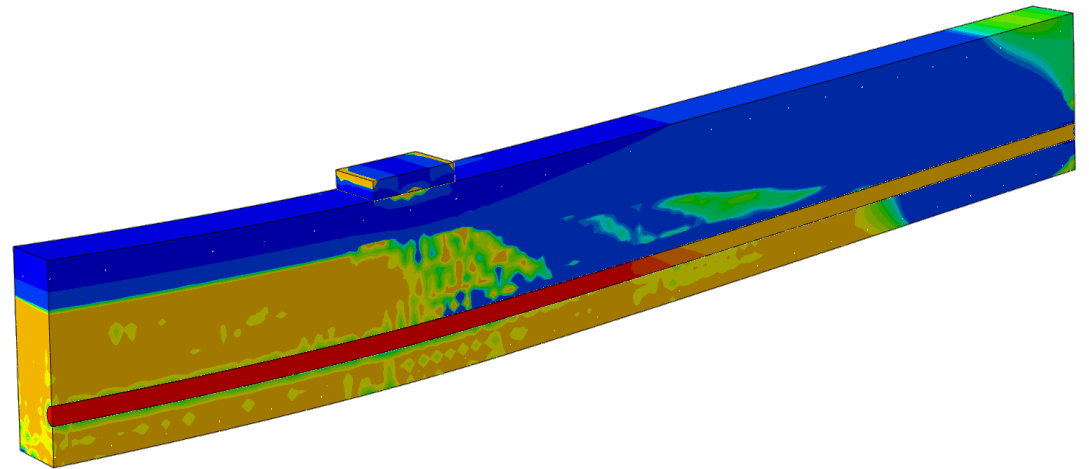
Concrete Damaged Plasticity

Elementer

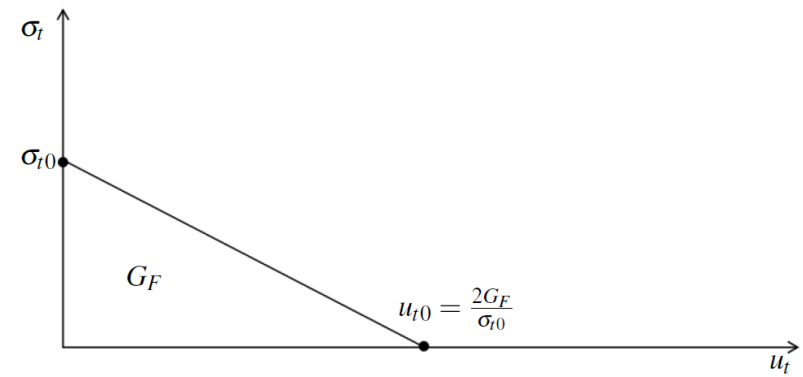
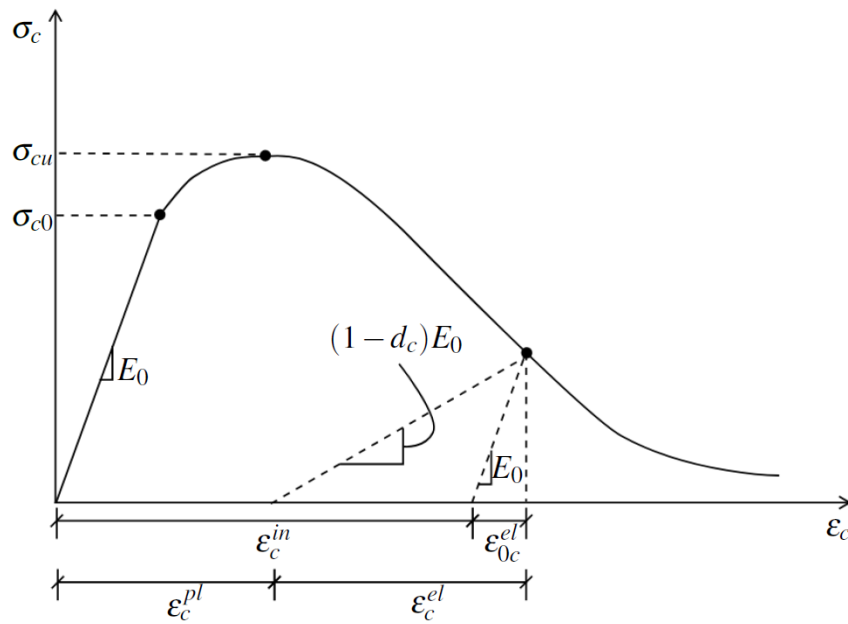
Randbetingelser

Resultater

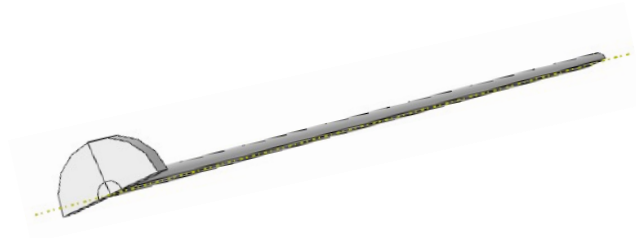
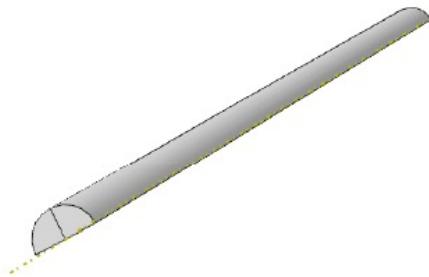
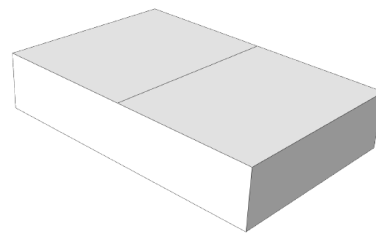
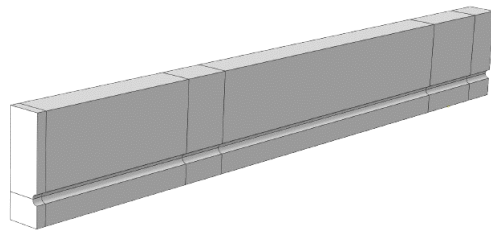
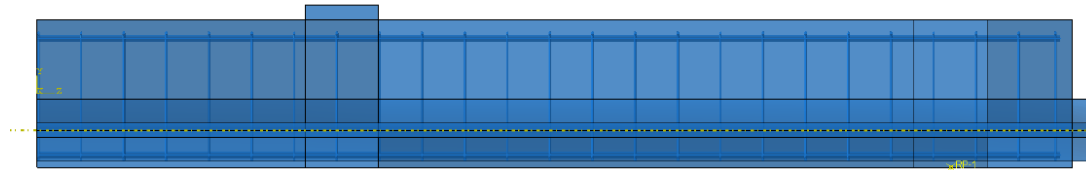
Parameter studie



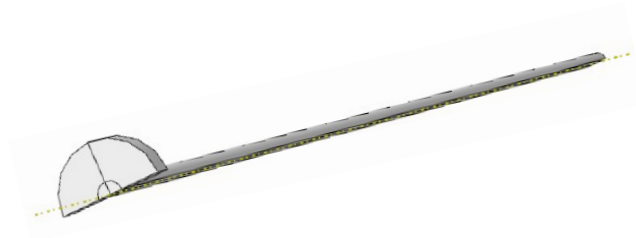
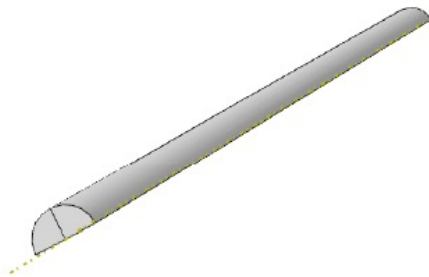
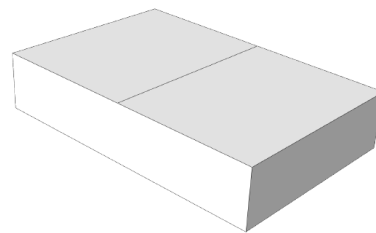
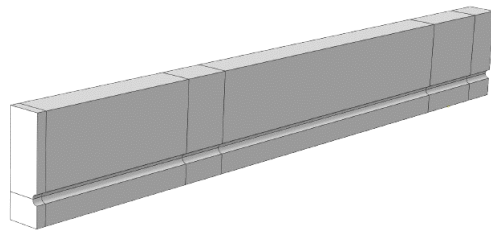
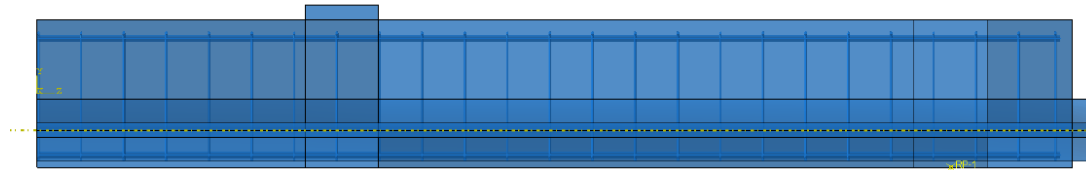
Concrete Damaged Plasticity



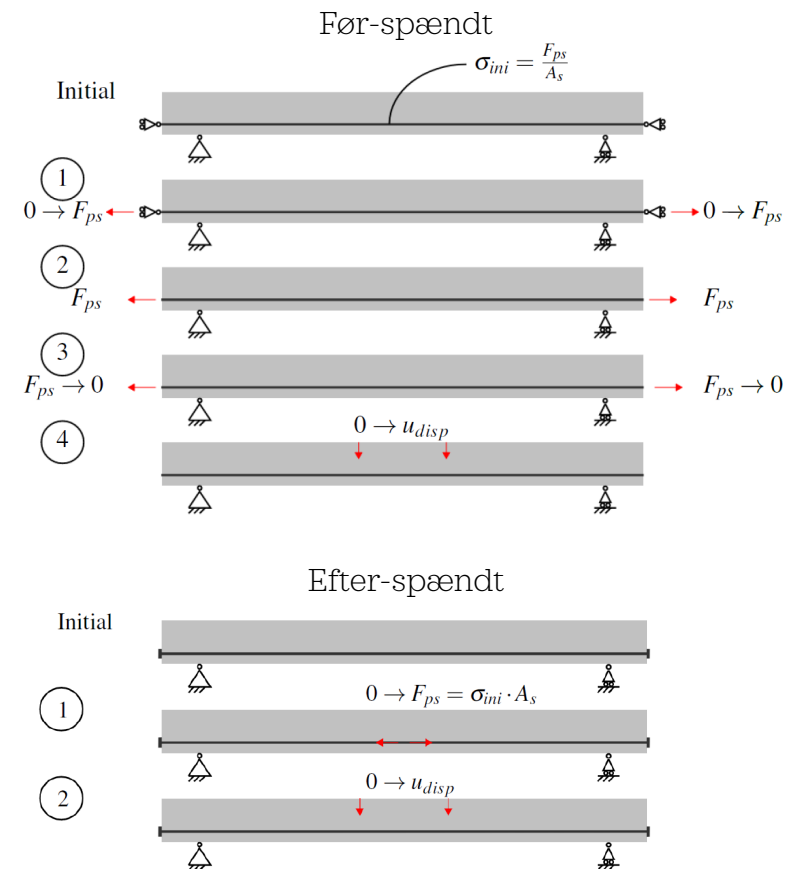
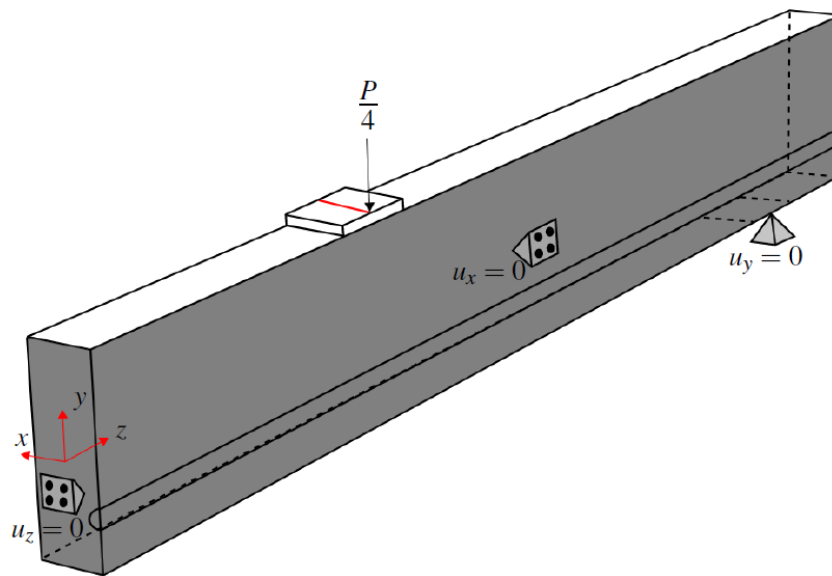
Elementer



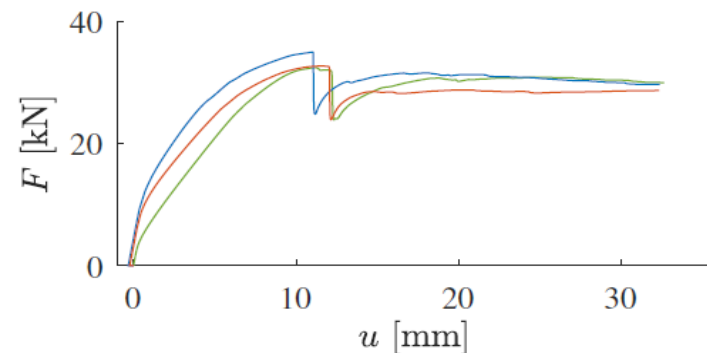
Elementer



Randbetingelser

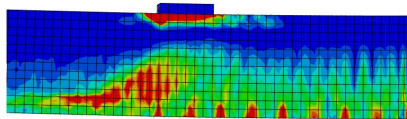


Resultater

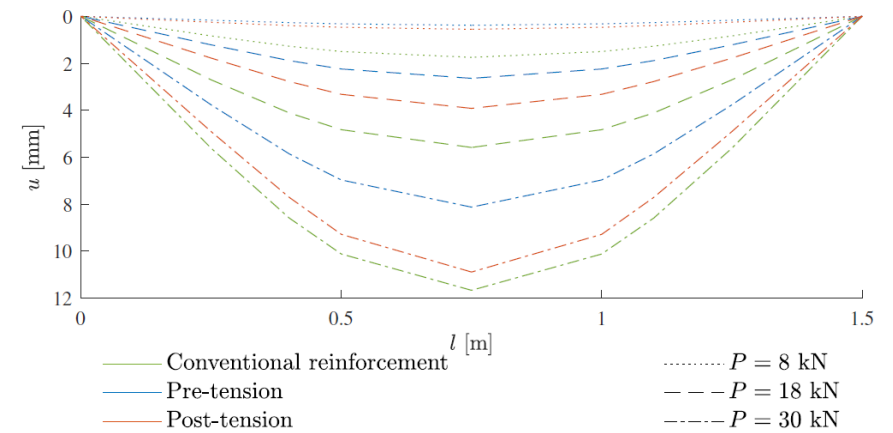
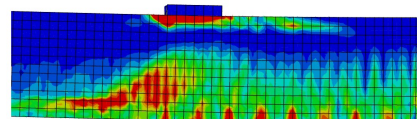


— Conventional reinforcement — Pre-tension — Post-tension

Før fald i last

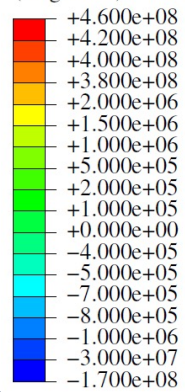


Efter fald i last

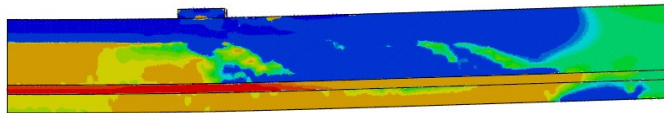


Spændinger i længde retningen

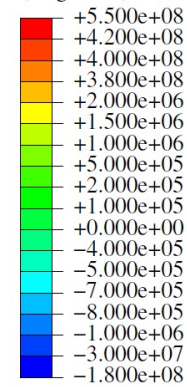
S, S33
(Avg: 75%)



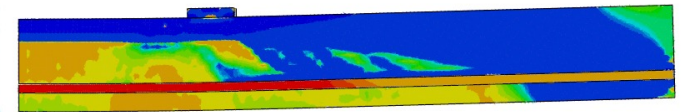
Slapt armeret



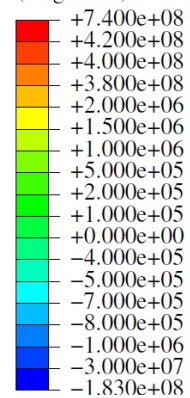
S, S33
(Avg: 75%)



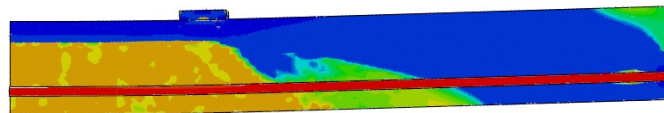
Før-spændt



S, S33
(Avg: 75%)

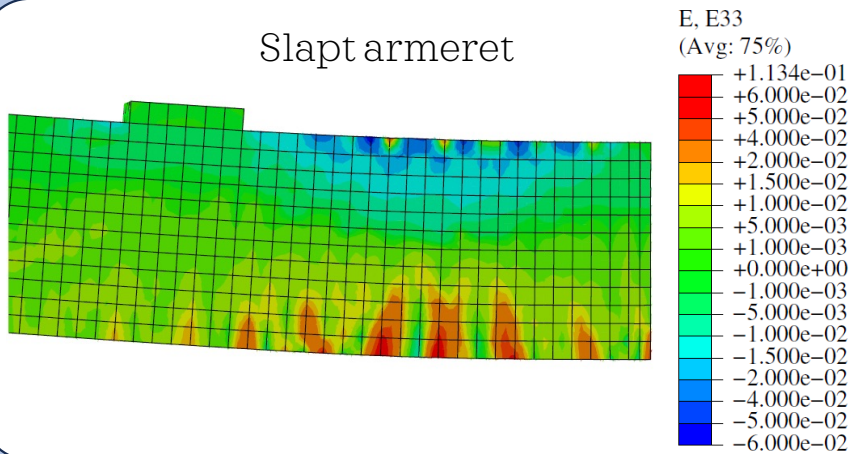


Efter-spændt

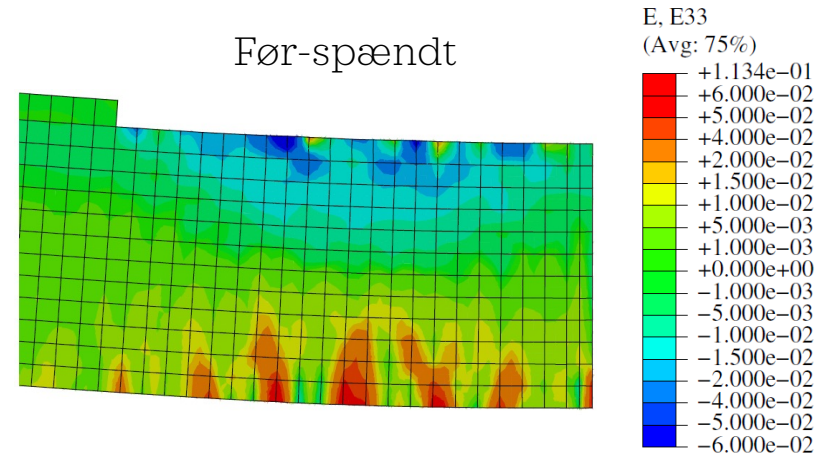


Tøjninger i længde retningen

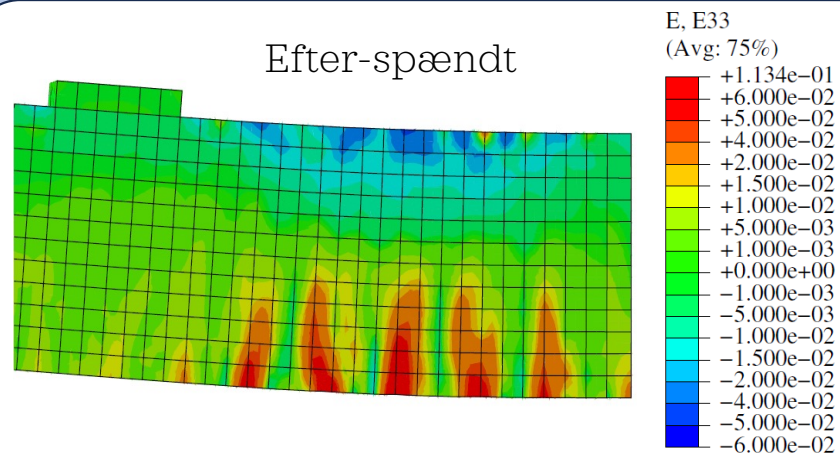
Slapt armeret



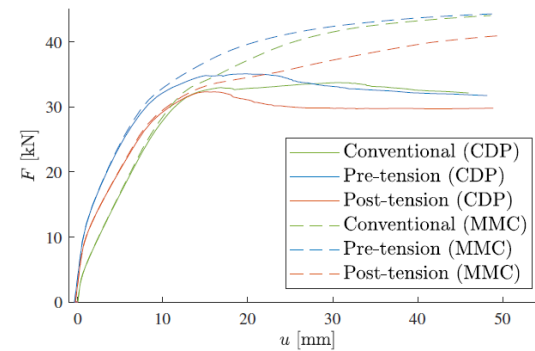
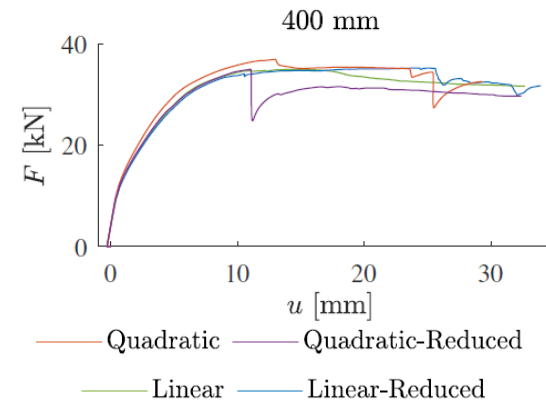
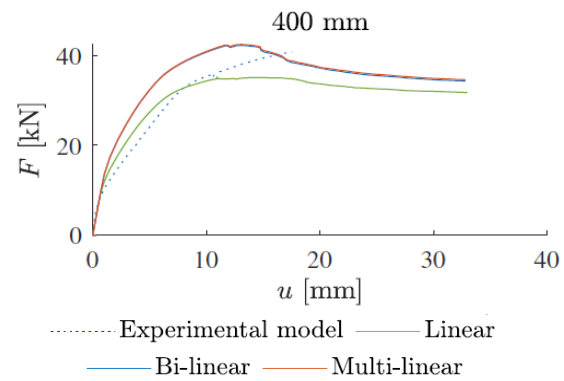
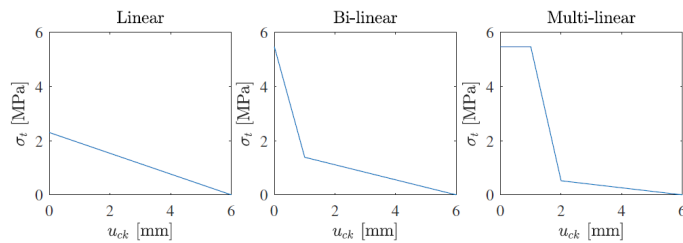
Før-spændt



Efter-spændt



Parameter studie



Semi-analytisk model

Idé og forudsætninger

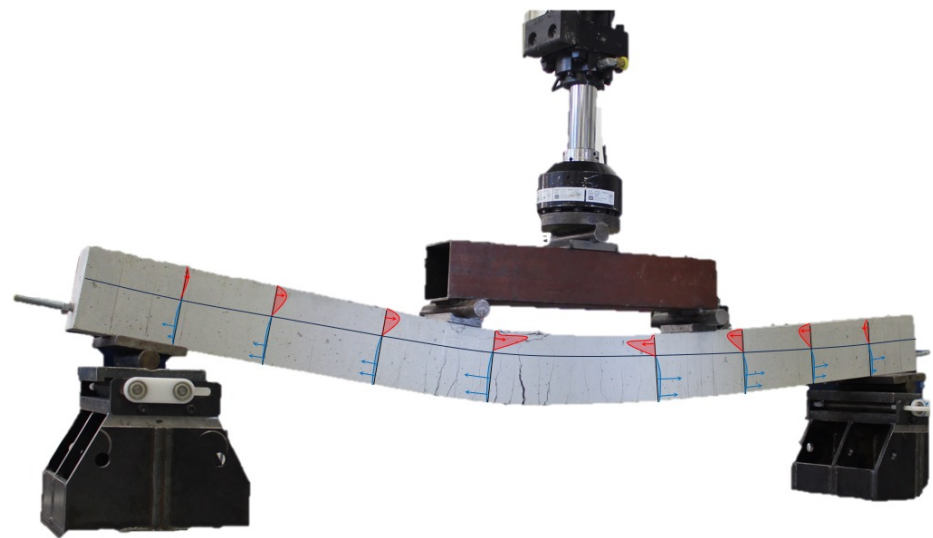
Beregningsgang

Moment-krumnings relationen

Virtuelt arbejdes princip

Modellering af træk

Output



Semi-analytisk model

Idé og forudsætninger

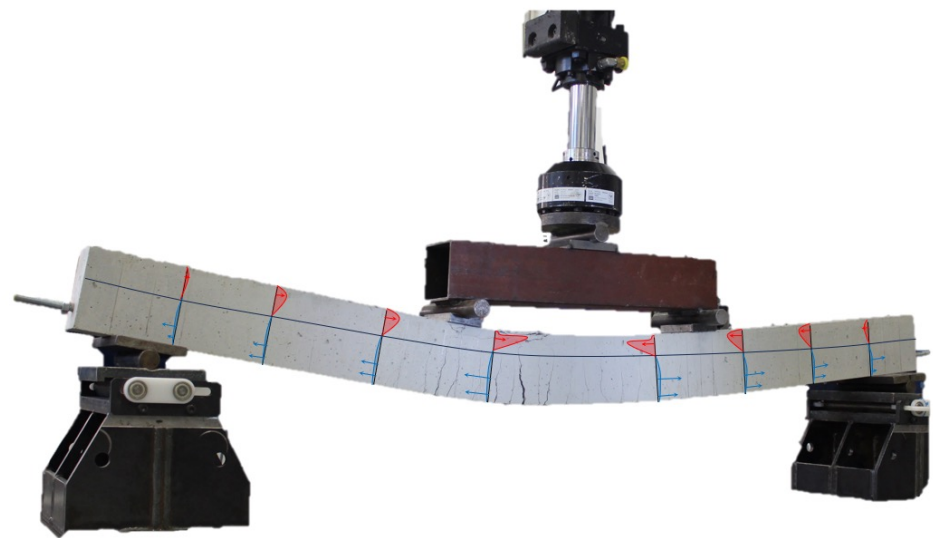
Beregningsgang

Moment-krumnings relationen

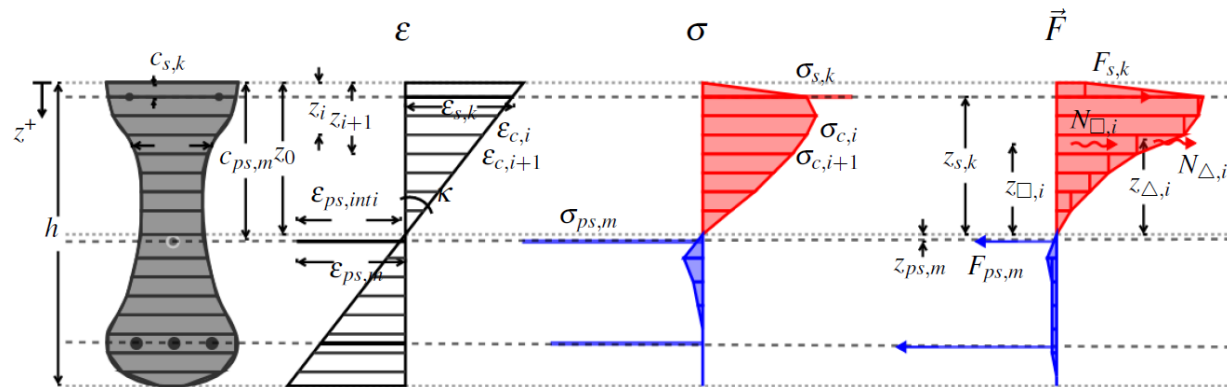
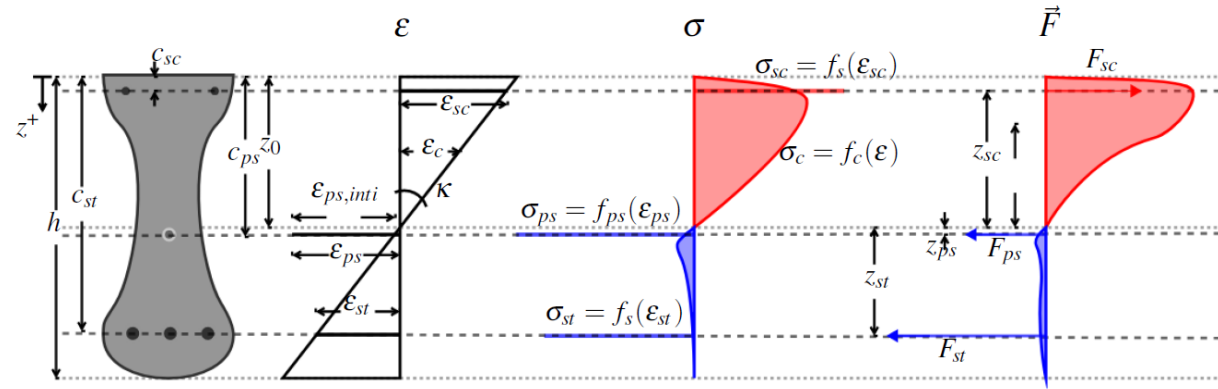
Virtuelt arbejdes princip

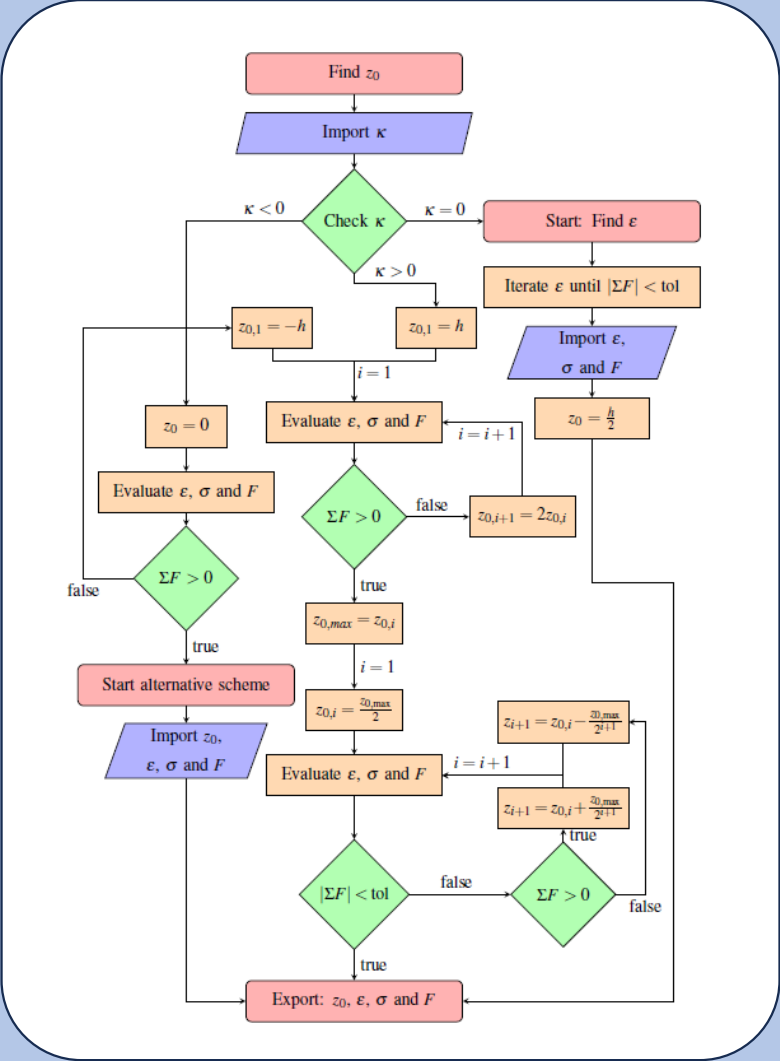
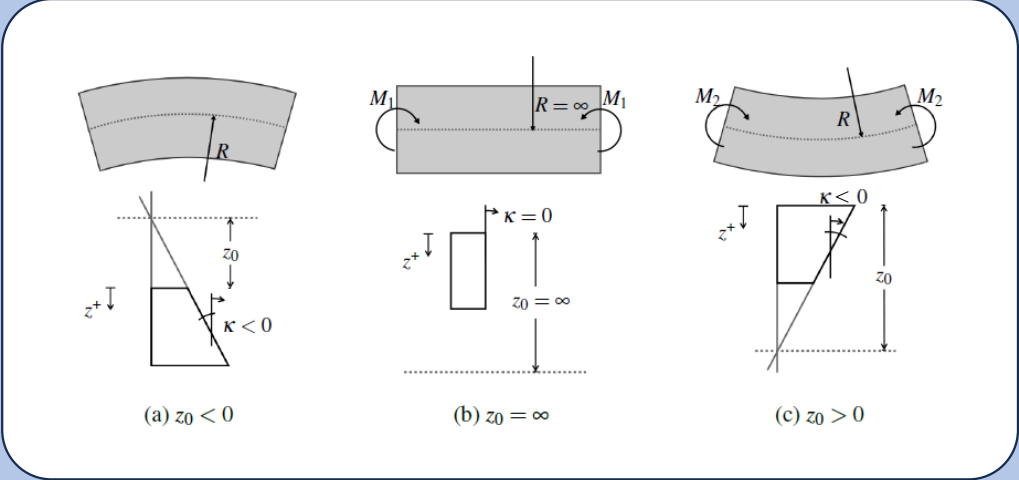
Modellering af træk

Output

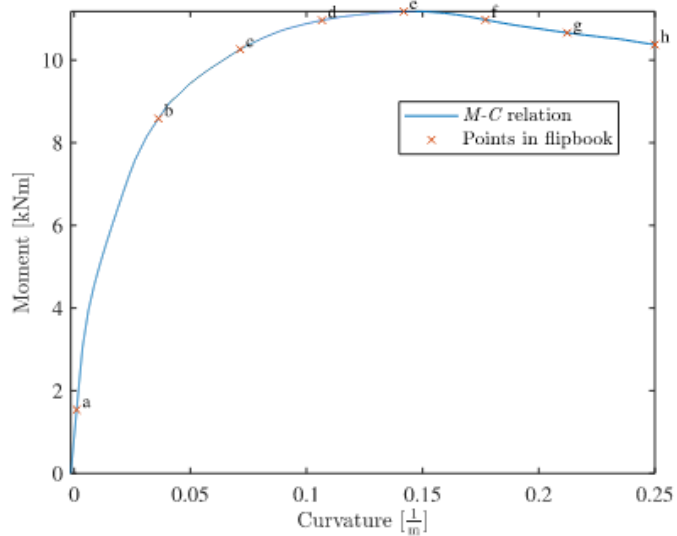


Idé og forudsætninger

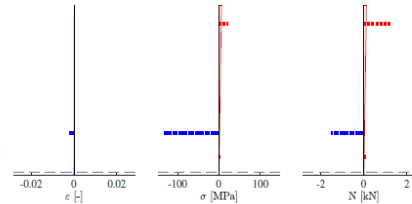




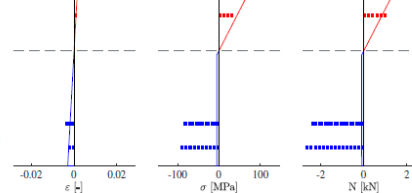
Moment-krumnings relationen



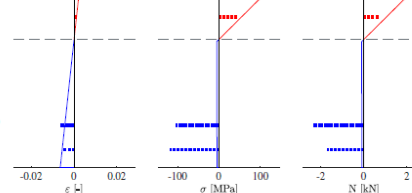
a)
 $M = 1.54 \text{ kNm}$
 $\kappa = 0.00 \frac{1}{m}$
 Scaling:
 $\sigma_s 1:1 \quad N_s 1:1$
 $\sigma_{ps} 1:2 \quad N_{ps} 1:20$



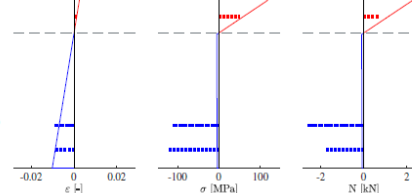
b)
 $M = 8.58 \text{ kNm}$
 $\kappa = 0.04 \frac{1}{m}$
 Scaling:
 $\sigma_s 1:5 \quad N_s 1:10$
 $\sigma_{ps} 1:5 \quad N_{ps} 1:20$



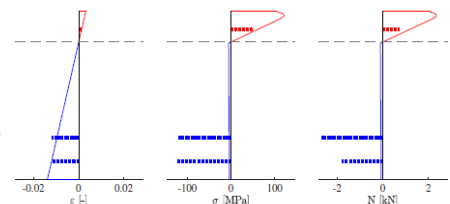
c)
 $M = 10.26 \text{ kNm}$
 $\kappa = 0.07 \frac{1}{m}$
 Scaling:
 $\sigma_s 1:5 \quad N_s 1:20$
 $\sigma_{ps} 1:5 \quad N_{ps} 1:25$



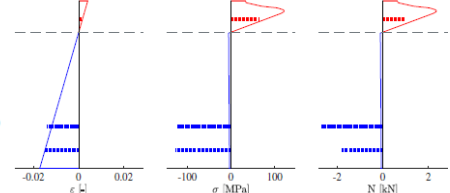
d)
 $M = 10.96 \text{ kNm}$
 $\kappa = 0.11 \frac{1}{m}$
 Scaling:
 $\sigma_s 1:5 \quad N_s 1:20$
 $\sigma_{ps} 1:5 \quad N_{ps} 1:25$



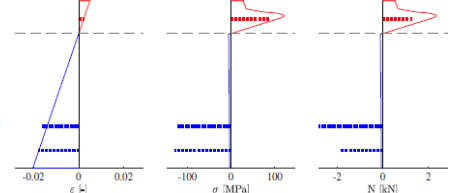
e)
 $M = 11.18 \text{ kNm}$
 $\kappa = 0.14 \frac{1}{m}$
 Scaling:
 $\sigma_s 1:5 \quad N_s 1:20$
 $\sigma_{ps} 1:5 \quad N_{ps} 1:25$



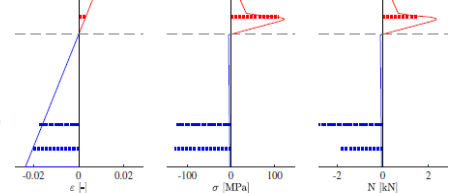
f)
 $M = 10.97 \text{ kNm}$
 $\kappa = 0.18 \frac{1}{m}$
 Scaling:
 $\sigma_s 1:5 \quad N_s 1:20$
 $\sigma_{ps} 1:5 \quad N_{ps} 1:25$



g)
 $M = 10.66 \text{ kNm}$
 $\kappa = 0.21 \frac{1}{m}$
 Scaling:
 $\sigma_s 1:5 \quad N_s 1:20$
 $\sigma_{ps} 1:5 \quad N_{ps} 1:25$

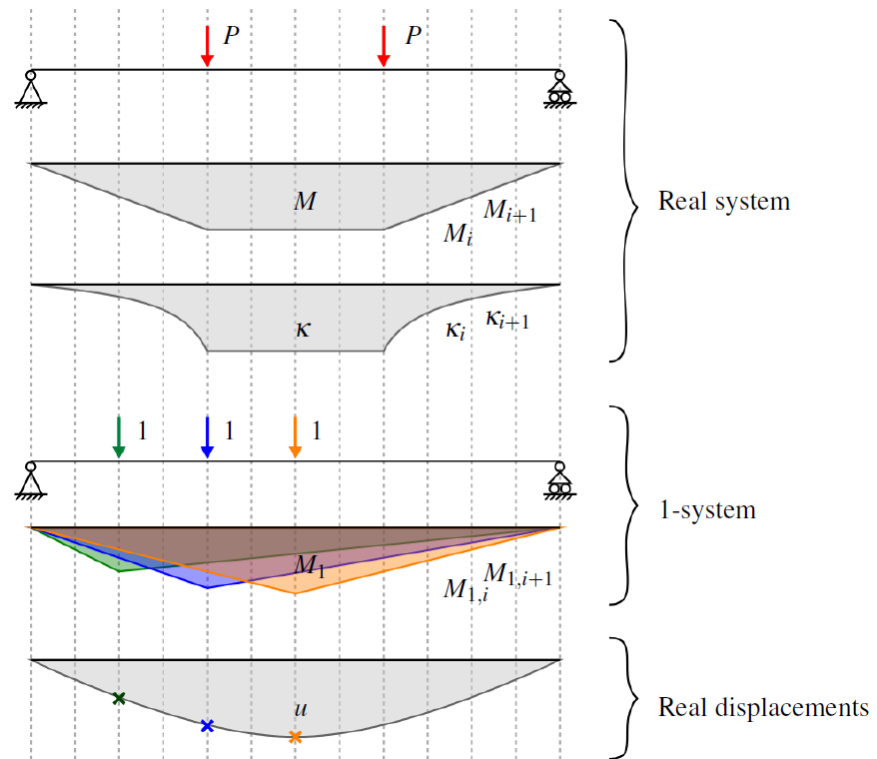


h)
 $M = 10.37 \text{ kNm}$
 $\kappa = 0.25 \frac{1}{m}$
 Scaling:
 $\sigma_s 1:5 \quad N_s 1:20$
 $\sigma_{ps} 1:5 \quad N_{ps} 1:25$



— Concrete Reinforcement --- Tendon

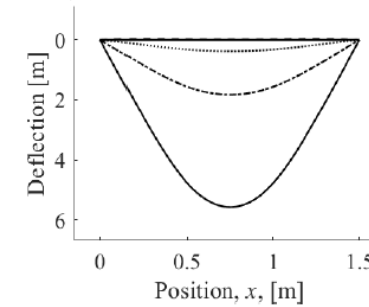
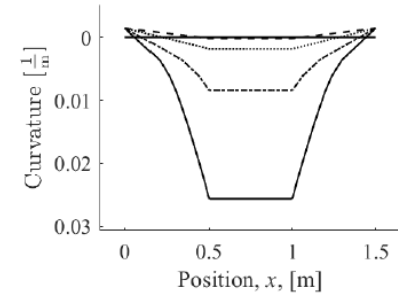
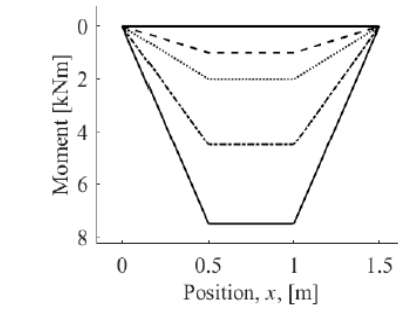
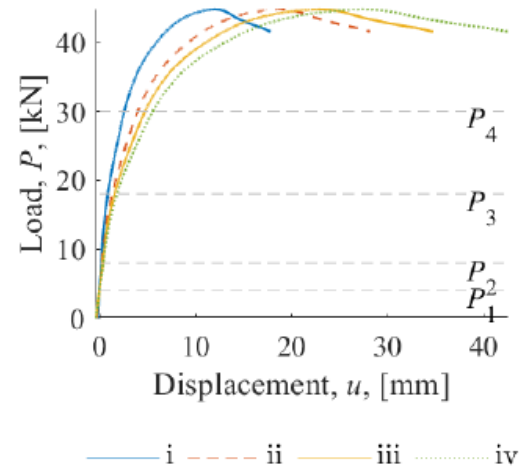
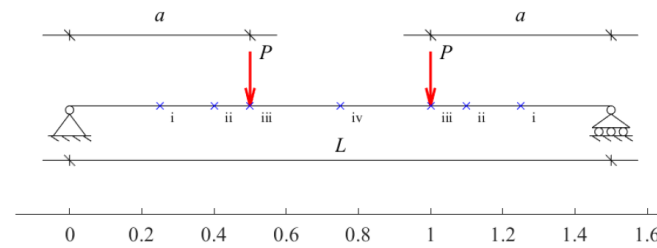
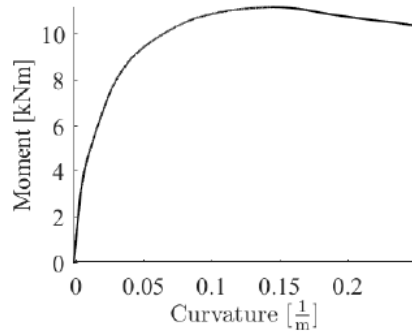
Virtuelt arbejdes princip



$$uP_1 = \int_L M_1(x) \kappa(x) dx$$

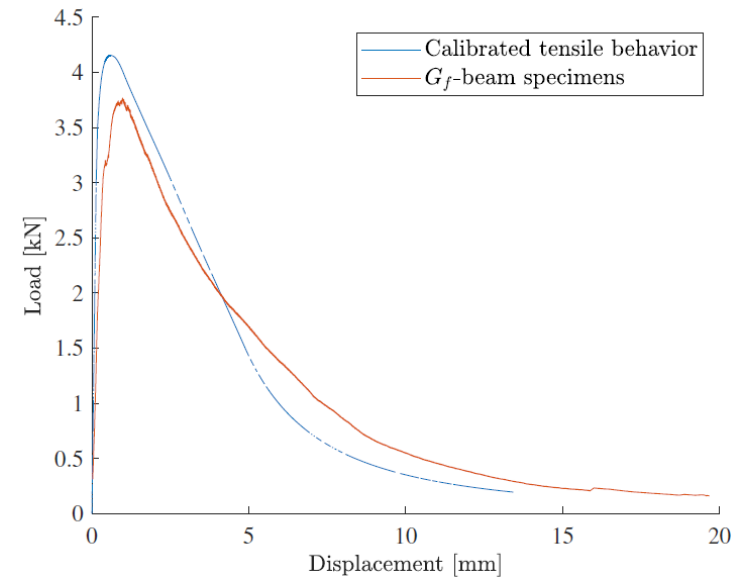
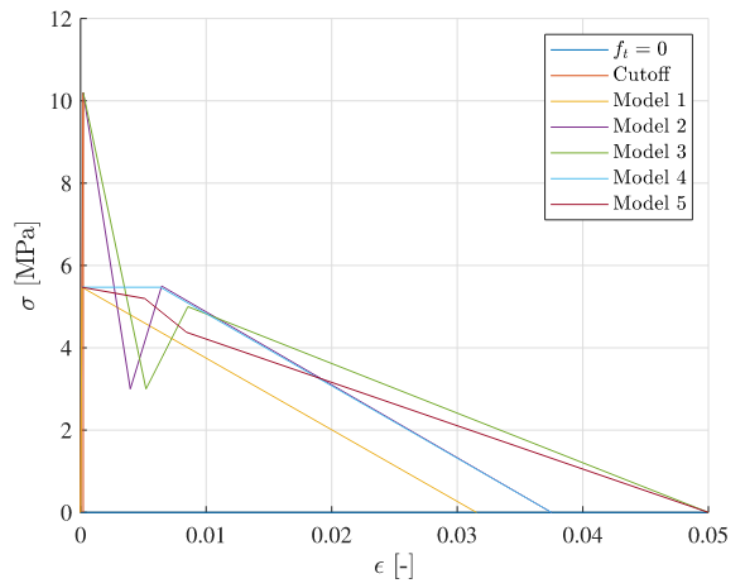
$$u_j P_{1,j} = \sum_{i=1}^{n-1} \frac{M_{1,i} + M_{1,i+1}}{2} \frac{\kappa_i + \kappa_{i+1}}{2} \Delta x$$

Output

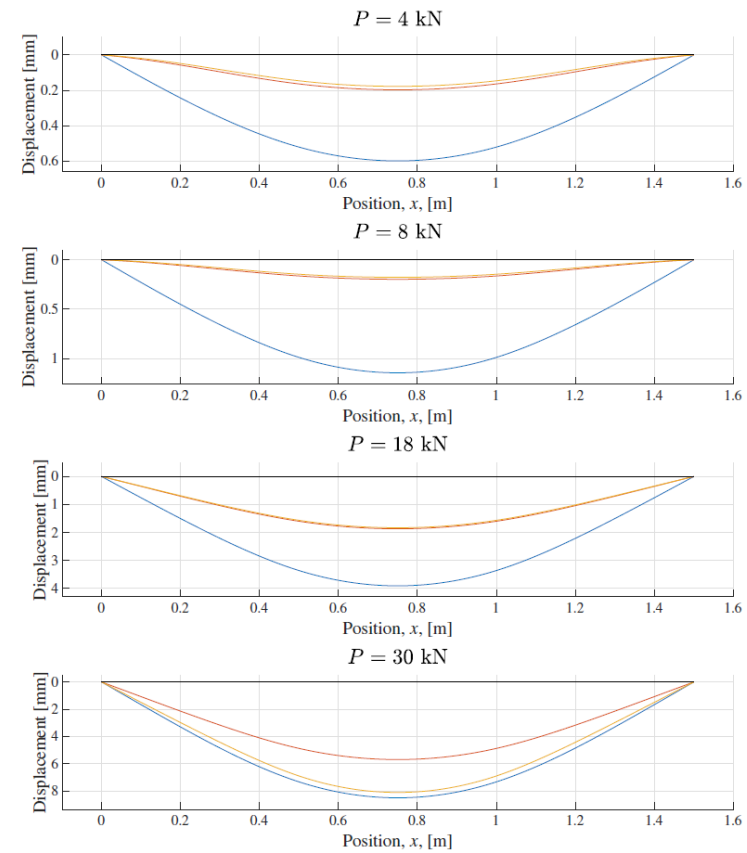
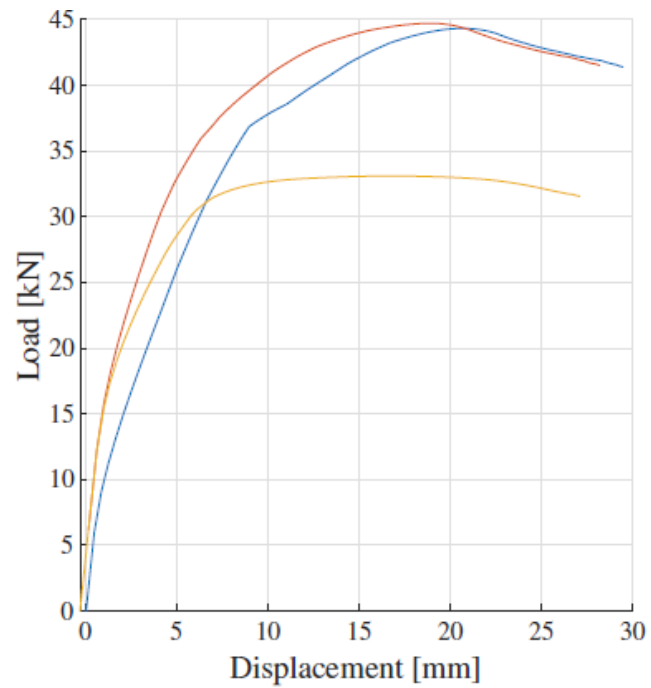


- $P_4 = 30$ kN
- - - $P_3 = 18$ kN
- $P_2 = 7.99$ kN
- - - $P_1 = 4$ kN

Modellering af træ



Resultater



— Non-prestressed — Pre-tensioned — Post-tensioned

Resultater

Arbejdskurver

Deformationsfigurer

Tøjningsfordeling

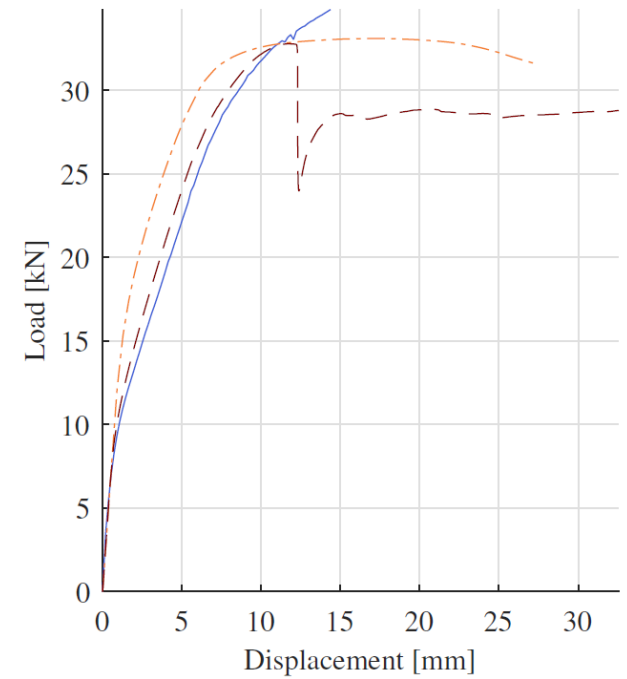
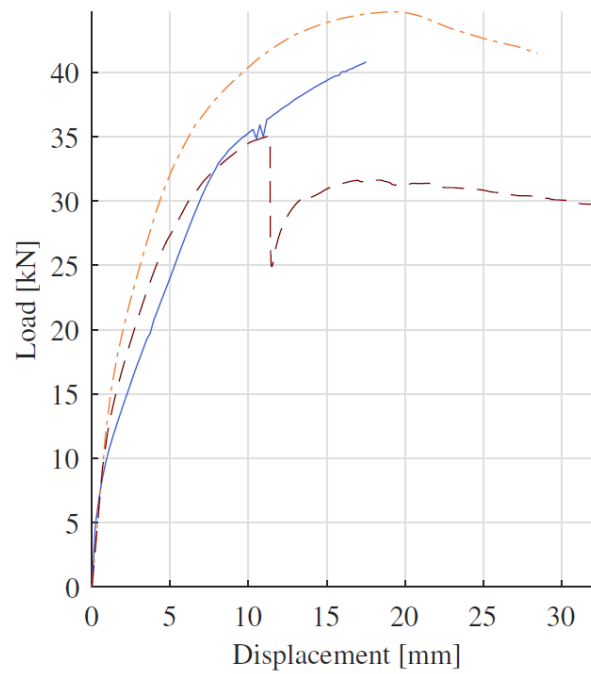
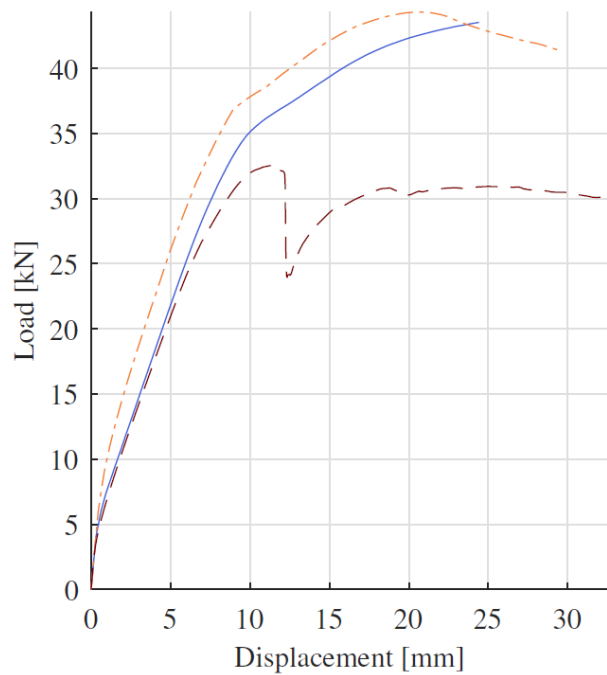
Resultater

Arbejdskurver

Deformationsfigurer

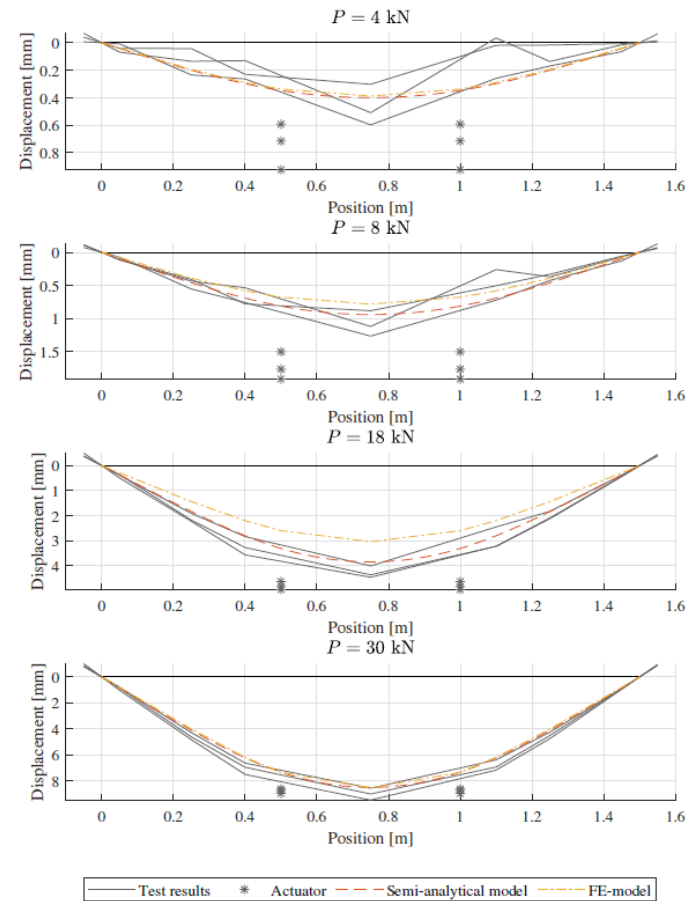
Tøjningsfordeling

Arbejdskruver

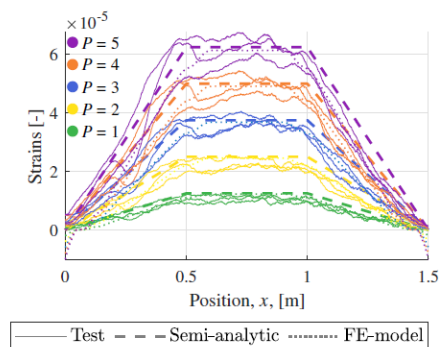
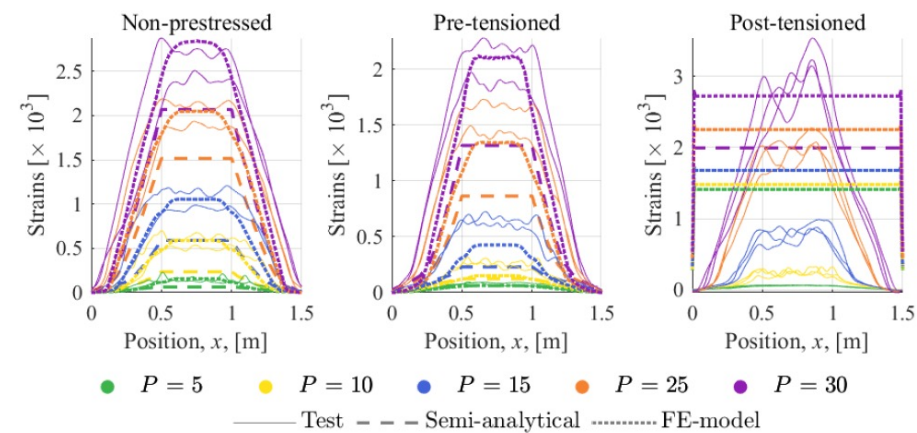
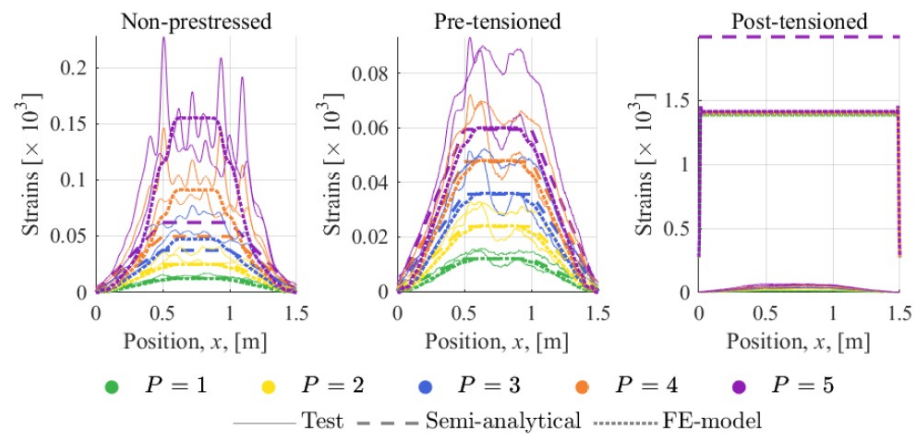


— Test results - - - Semi-analytical model - - - FE-model

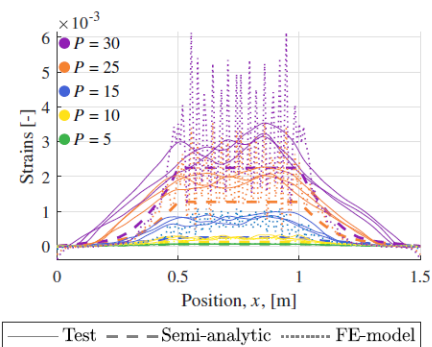
Deformationsfigurer



Tøjningsfordeling



(a) 1 kN - 5 kN



(b) 5 kN - 30 kN

Konklusion

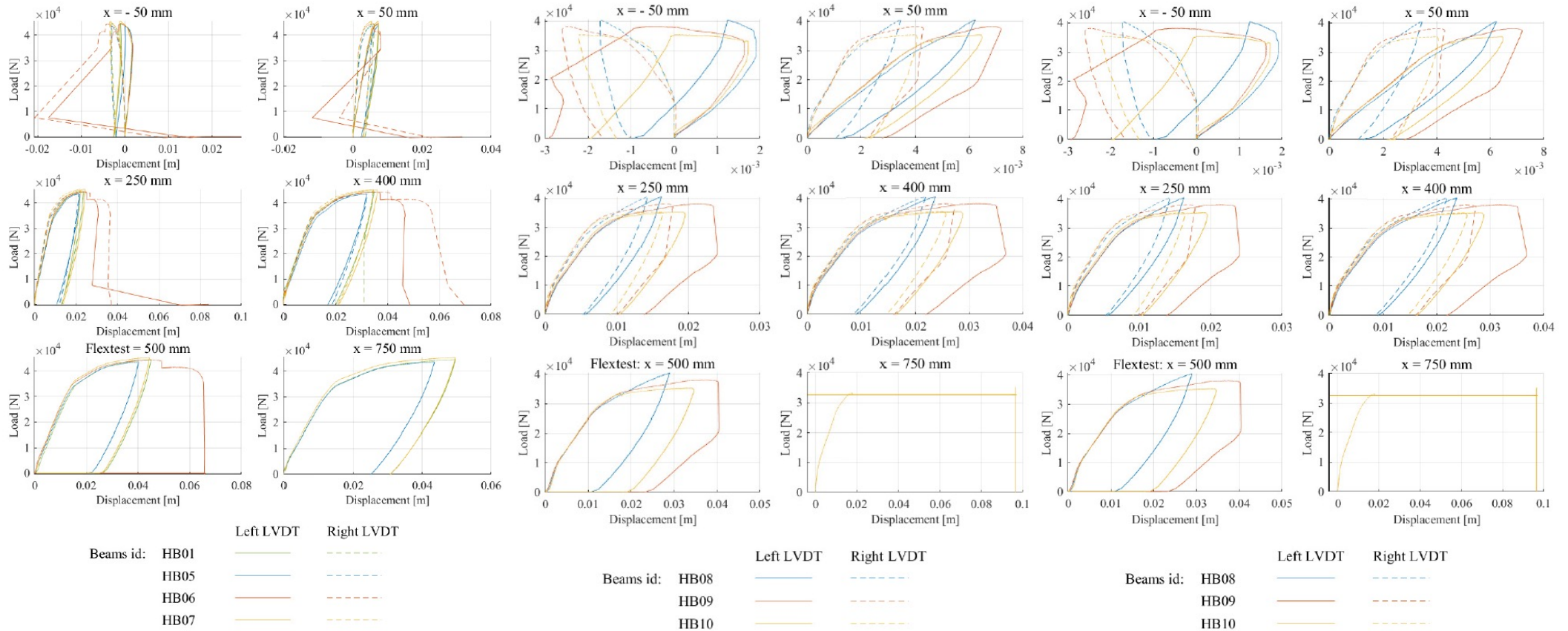
God overensstemmelse for den første del af arbejds kruven

Væsentlig stivheds forskel på slapt armerede og opspændte konstruktioner

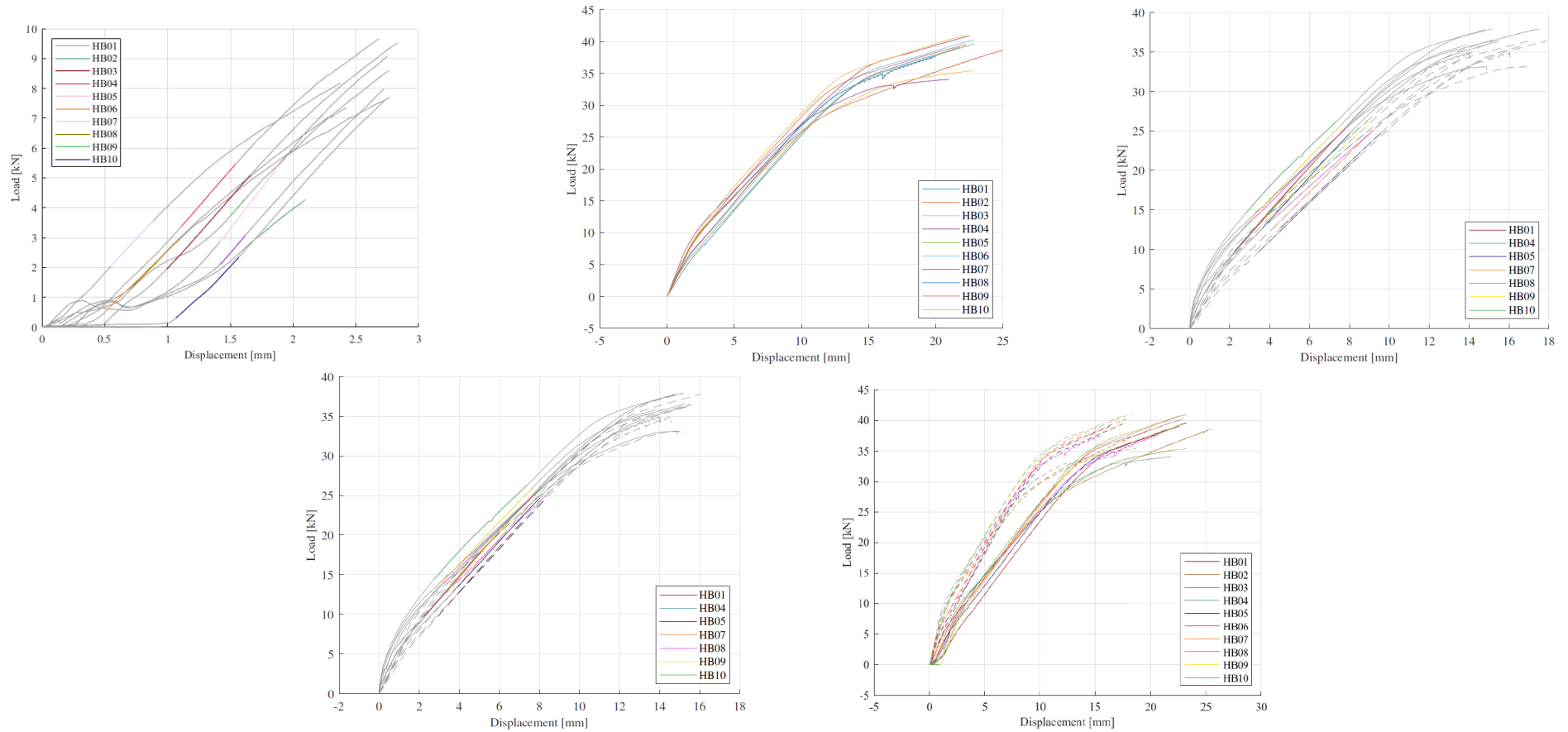
Modelleringsmetoderne kan bruges i videre udvikling

Tak

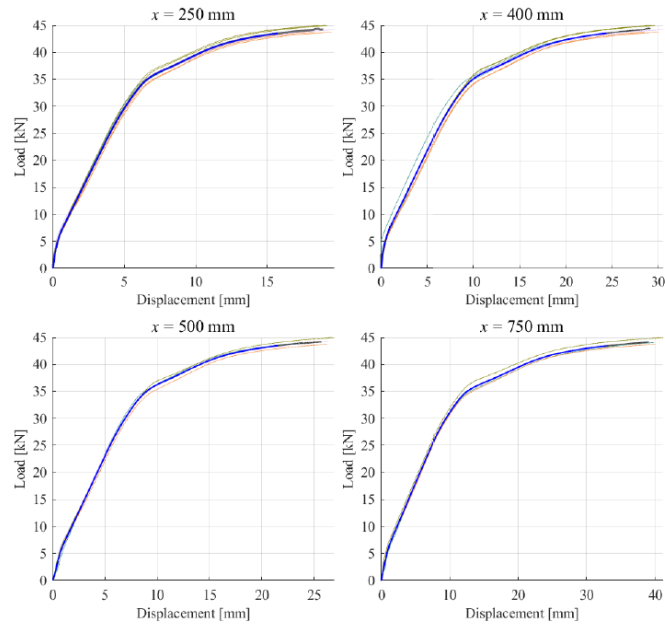
Bjælkeforsøg resultater



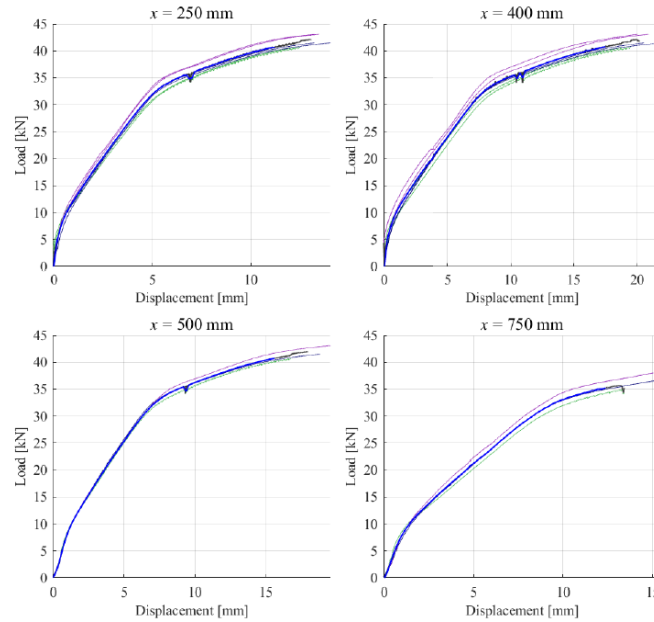
Bjælkeforsøg resultater



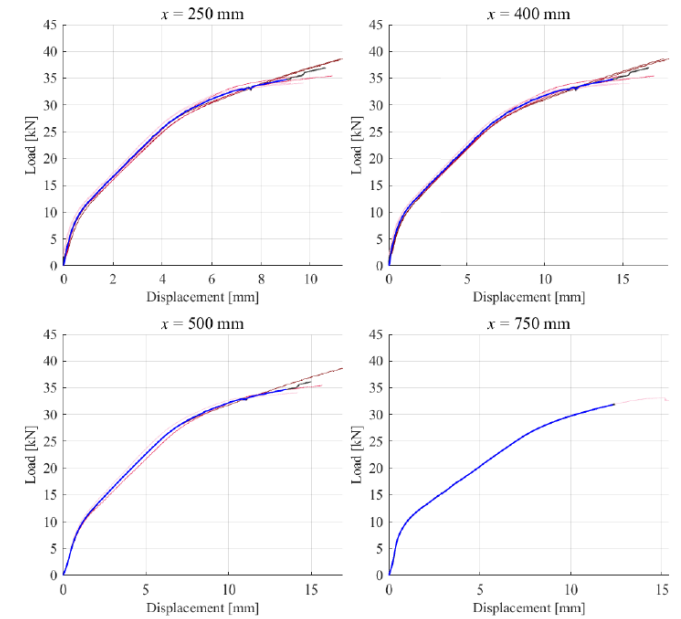
Bjælkeforsøg resultater



HB01 ● HB05 ● HB06 ● HB07 ●
Section mean ●

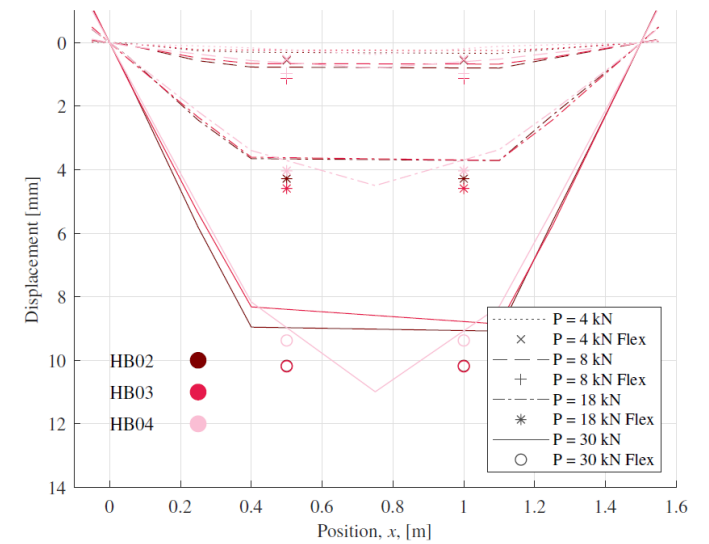
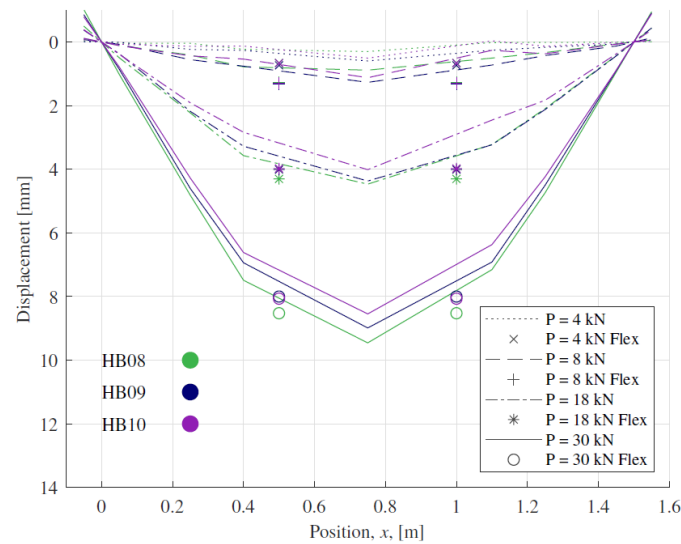
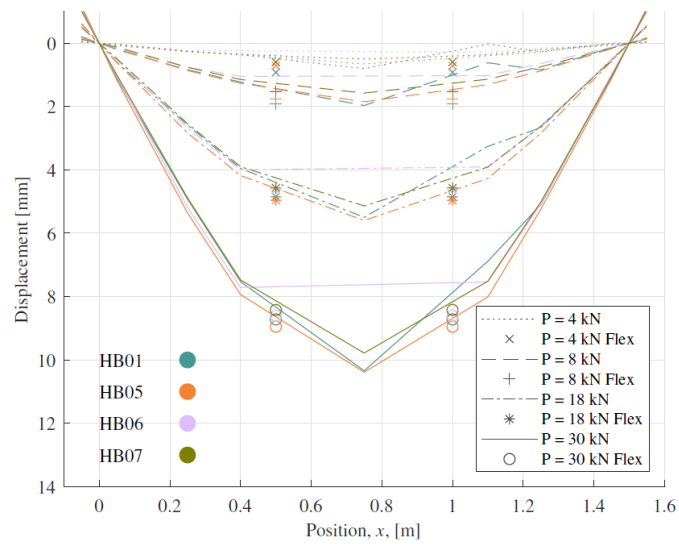


HB08 ● HB09 ● HB10 ●
Section mean ●

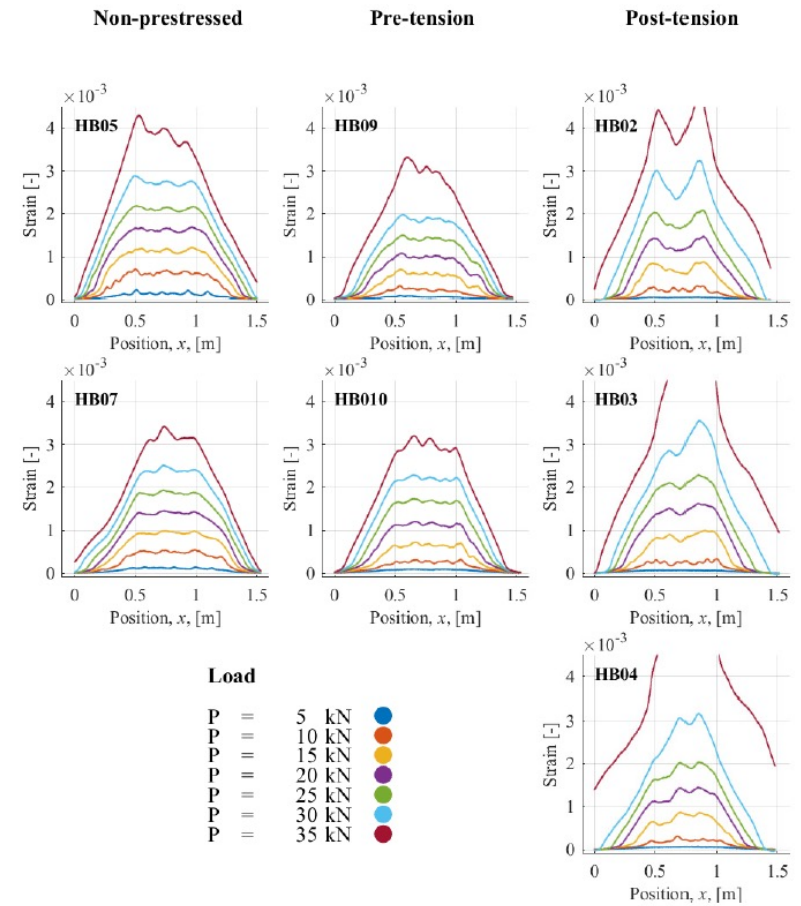
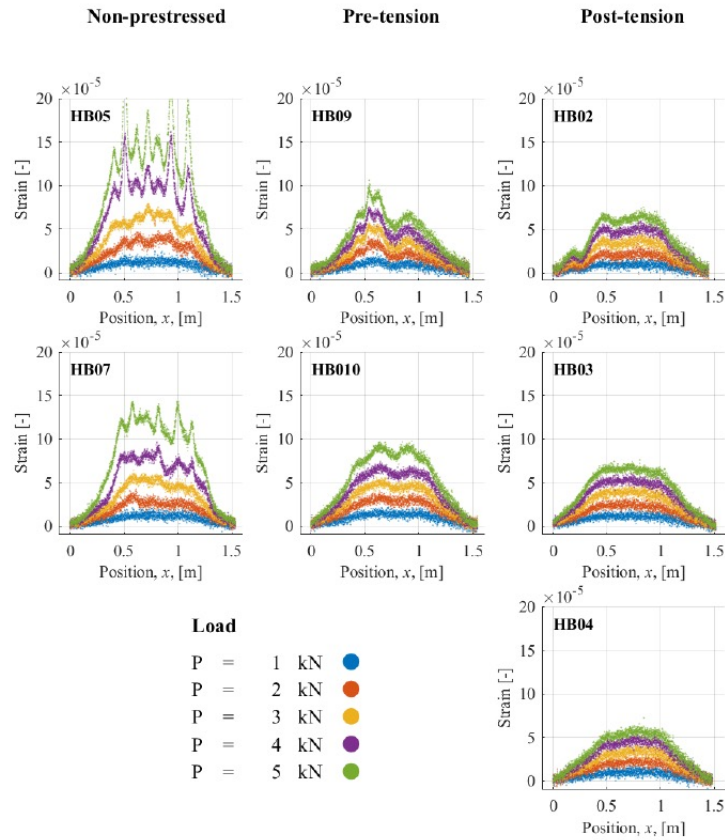


HB02 ● HB03 ● HB04 ●
Section mean ●

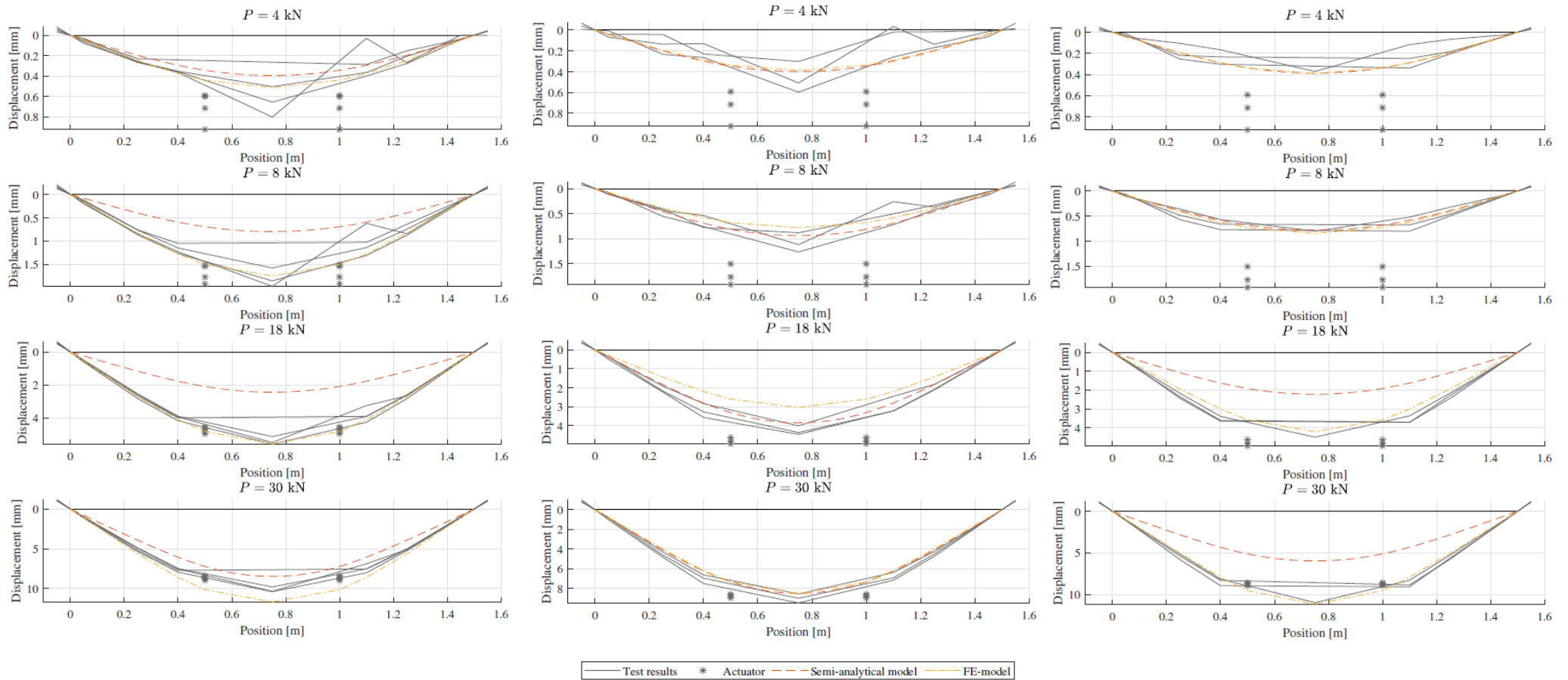
Bjælkeforsøg resultater



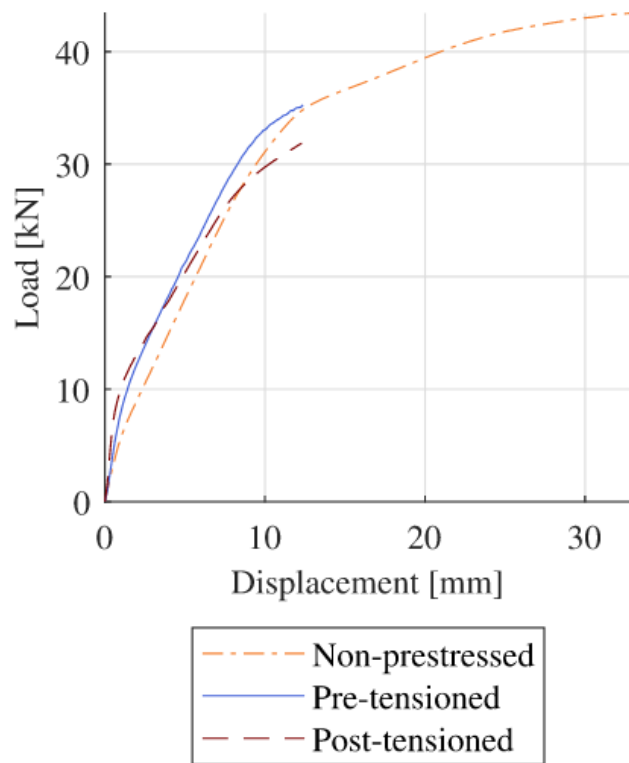
Bjælkeforsøg resultater



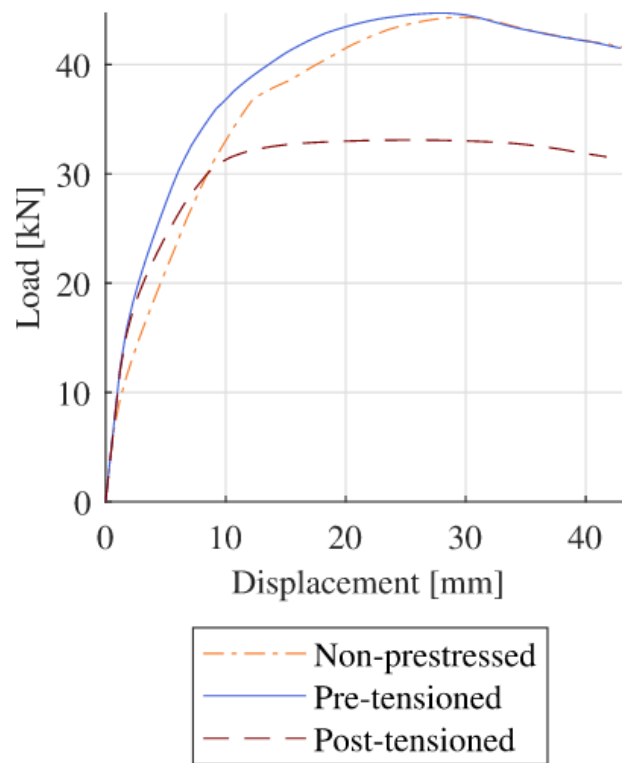
Resultat sammenligning



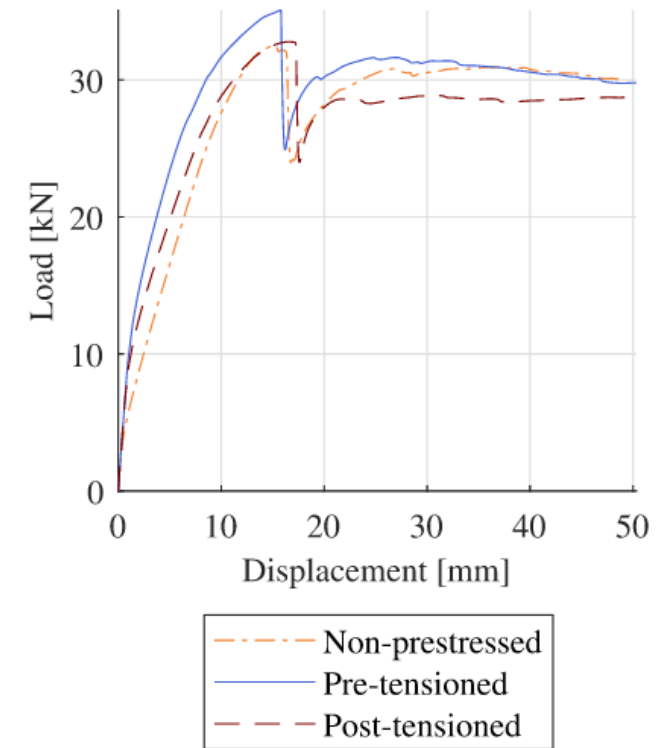
Resultat sammenligning



(a) Experimental campaign



(b) Semi-analytical



(c) FE-model